



**POLITECNICO**  
MILANO 1863

6<sup>th</sup> Two-Day Meeting on Propulsion Simulations using OpenFOAM technology

# **Accelerating CFD simulations of reactive flows through Cell Agglomeration and Adaptive Chemistry techniques**

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and Chemical Kinetics

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and Chemical Engineering "G. Natta"





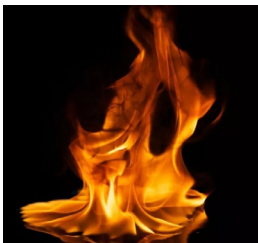
Real fuels and surrogates  
synergistic effects among the  
different components



Biofuels  
bioalcohols, biodiesel, green  
diesel, bioethers

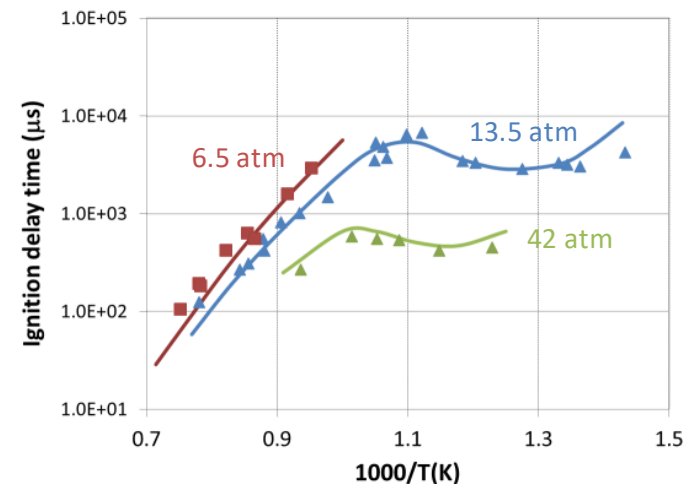


Pollutant emissions  
NO<sub>x</sub>, SO<sub>x</sub>, PAHs, soot



Complex phenomena  
Chemical instabilities, NTC, etc.

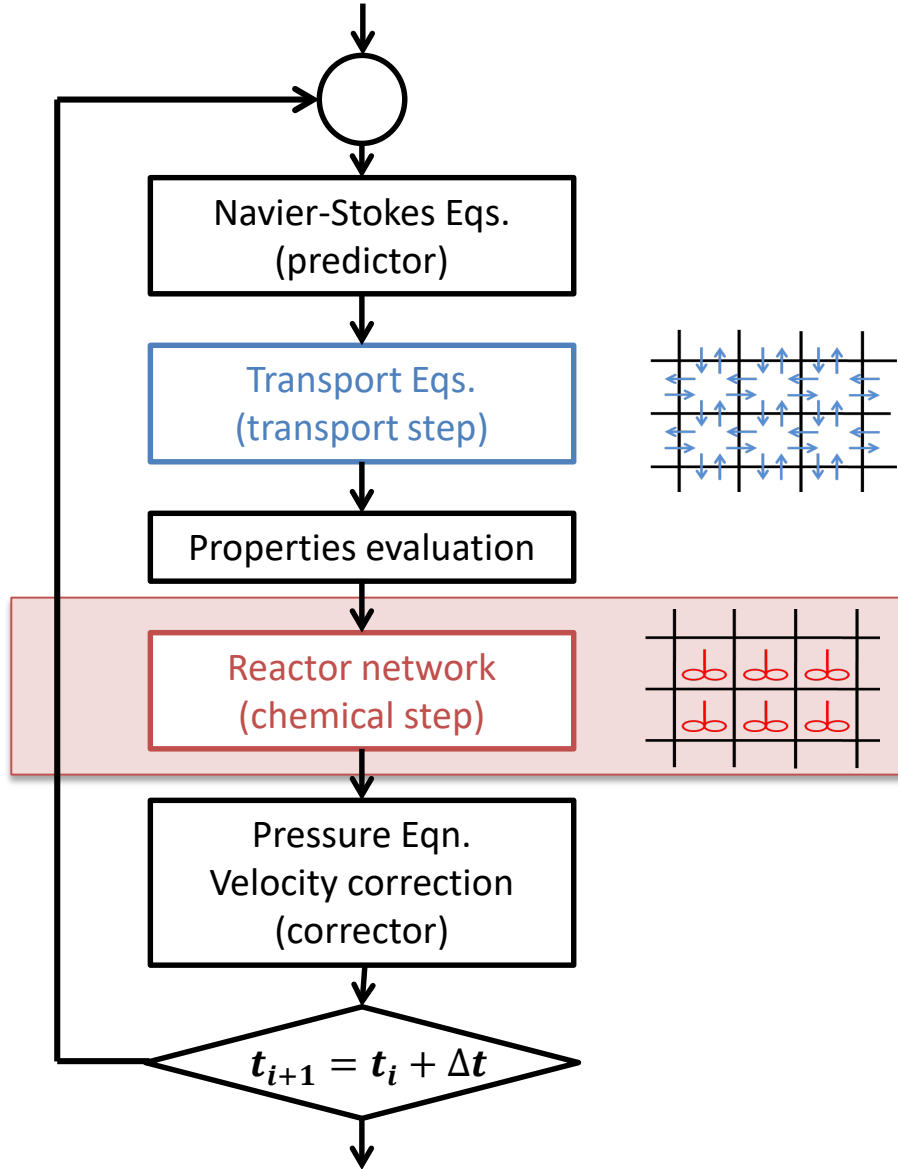
## Negative temperature Coefficients (NTC)



Experimental data from:

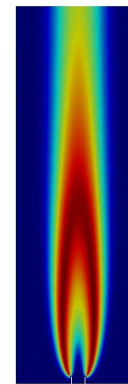
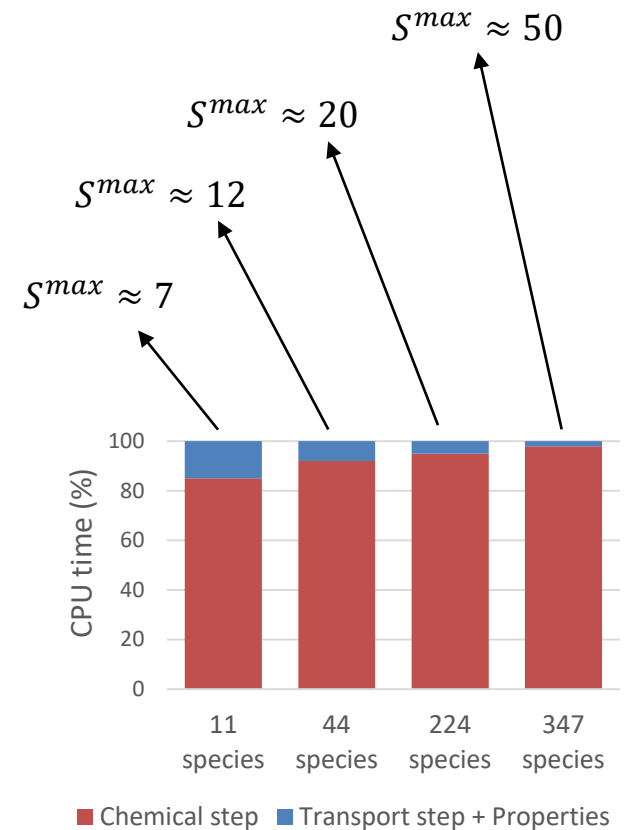
**Ciezki H.K. and Adomeit G.,** *Shock-tube investigation of self-ignition of n-heptane-air mixtures under engine relevant conditions*, Combustion and Flame 93 p. 421–433 (1993)

# Operator splitting: transport vs chemistry



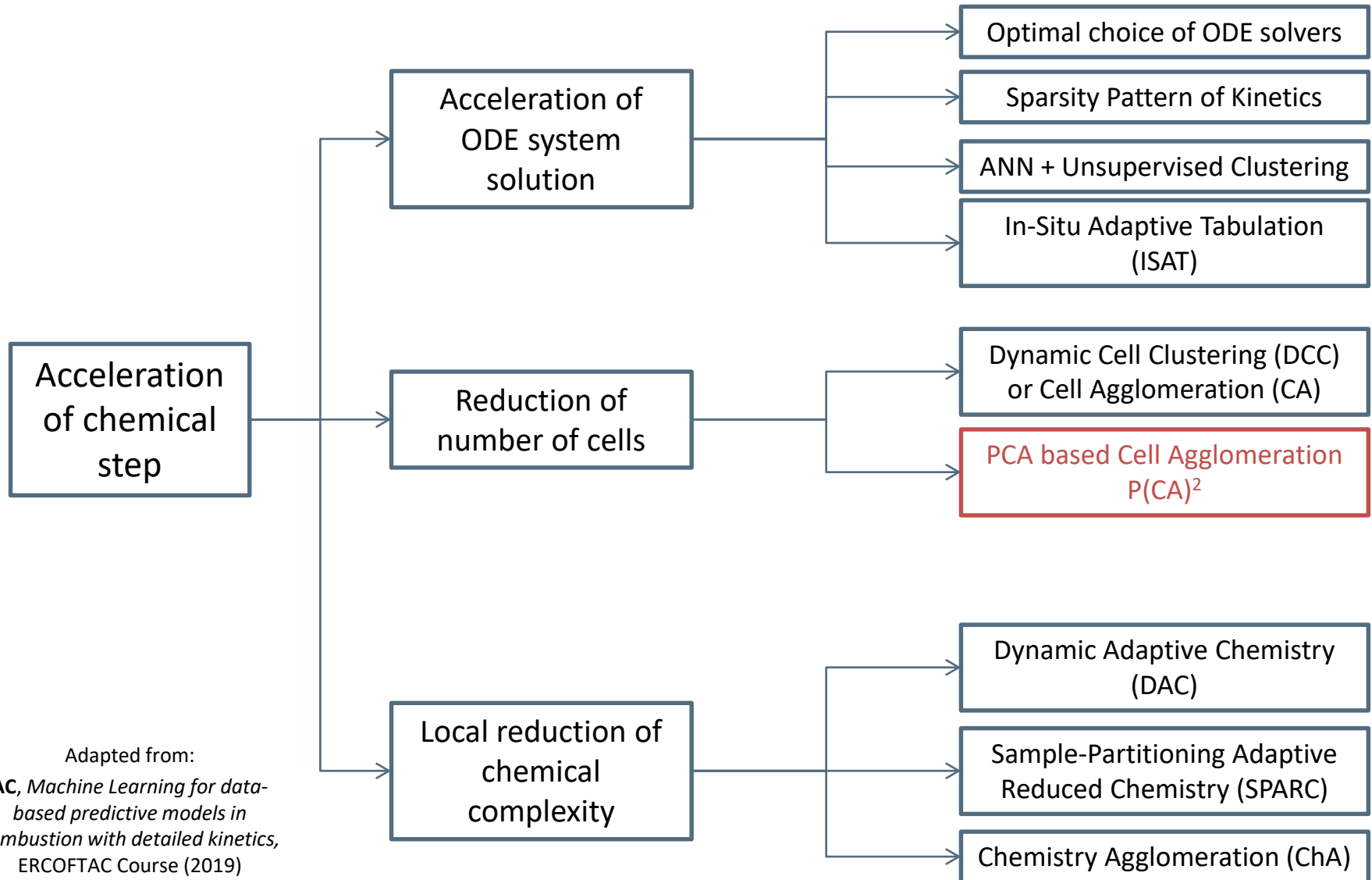
Maximum theoretical speed-up:

$$S^{max} = \frac{1}{1 - C_{chem}}$$



Pulsating laminar coflow flame

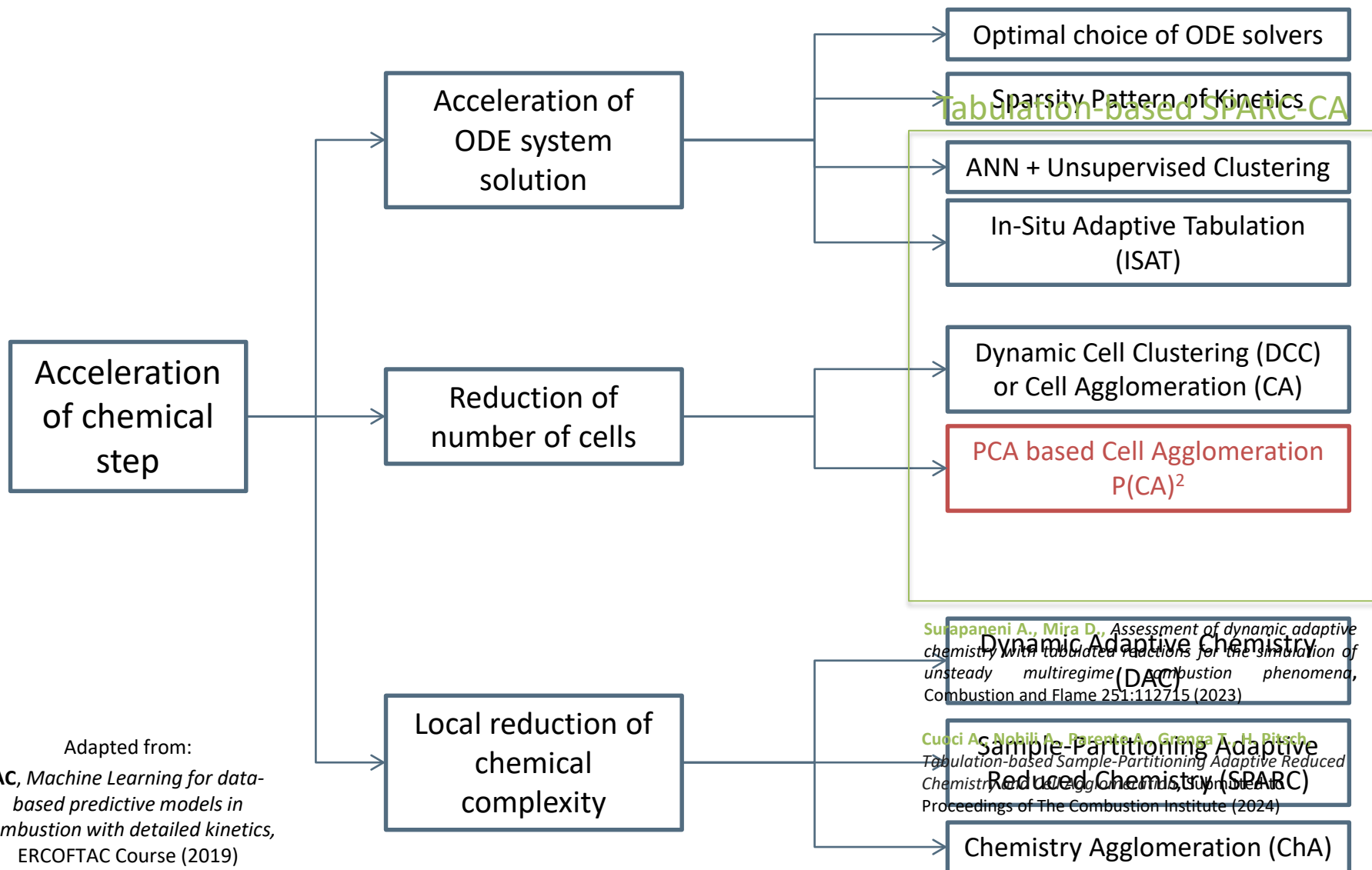
# Acceleration of chemical step (I)



Adapted from:  
**AC**, *Machine Learning for data-based predictive models in combustion with detailed kinetics*,  
ERCOFTAC Course (2019)



# Acceleration of chemical step (II)



Surapaneni A., Mira D., Assessment of dynamic adaptive chemistry with tabulated reactions for the simulation of unsteady multiregime combustion phenomena, Combustion and Flame 251:112715 (2023)

Cuoci A., Nobili A., Parente A., Granga T., H. Bittsch Tabulation-based Sample-Partitioning Adaptive Reduced Chemistry and Cell Agglomeration, Symposium on Proceedings of The Combustion Institute (2024)

## 1. $P(CA)^2$ : PCA-based Cell Agglomeration $P(CA)^2$

- Dynamic Cell Agglomeration and PCA
- Pulsating laminar coflow flame



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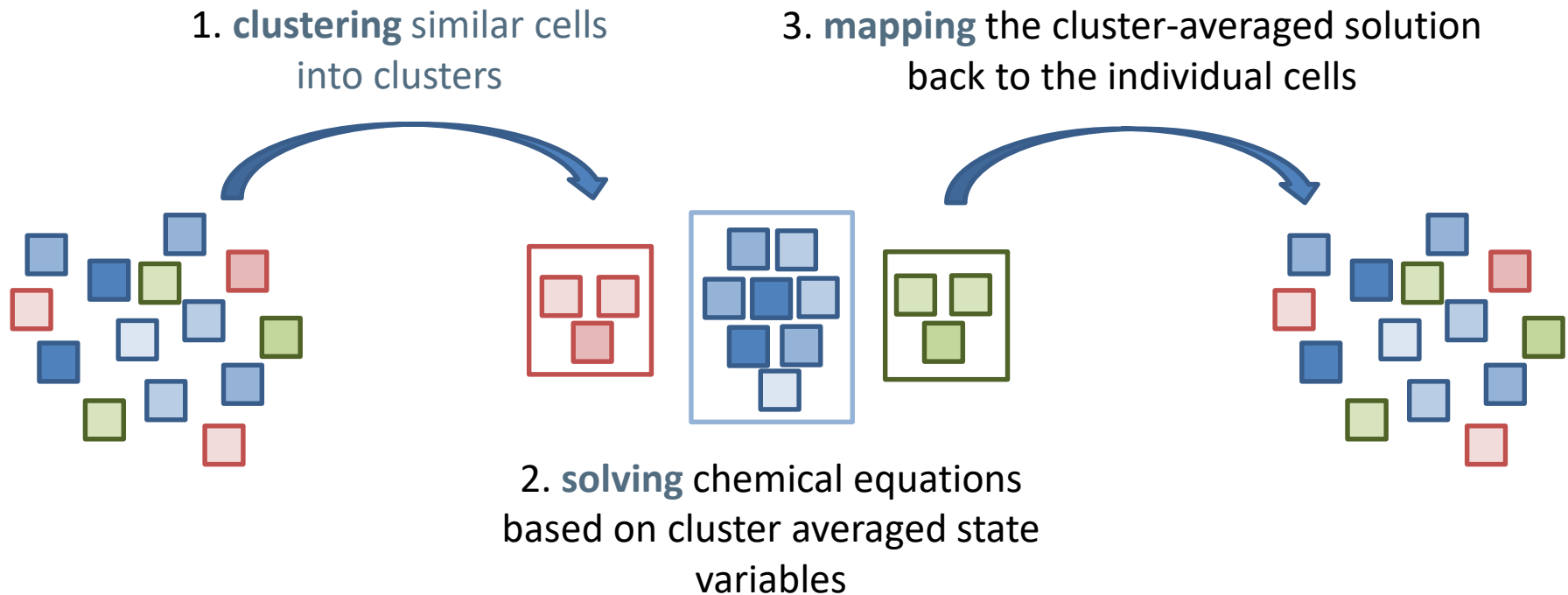


## 2. Tabulation-based SPARC-CA

- Temporally-evolving planar jet-flame
- 2D turbulent non-premixed flame including soot chemistry



**Dynamic Cell Agglomeration (DCA)** dynamically agglomerates regions of the domain that have **similar thermochemical conditions**.

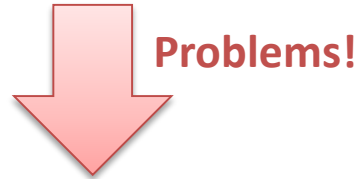
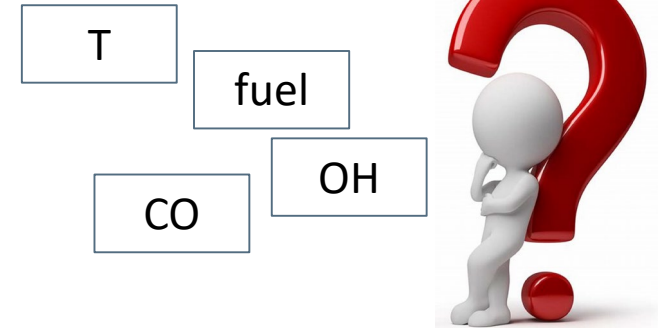


Liang et al., Combustion Science and Technology 181(11), p.1345-1371 (2009)

How to define/identify **similar thermochemical conditions**?

## Selection of *features*

A natural choice is **temperature** and a limited number of **key-species**



1. most abundant species are **not always the optimal choice**
2. **slowly-forming pollutants** (such as NO<sub>x</sub> or soot) make the selection of proper features more complex
3. it is difficult to identify **a priori** the optimal subset of species



**PCA (Principal Component Analysis)** to dynamically identify the optimal set of relevant features, evolving in time, following the evolution of combustion process

Current complete  
thermochemical state

$$\mathbf{X} = \begin{bmatrix} T_1 & Y_{1,1} & \dots & Y_{1,NS} \\ T_2 & Y_{2,1} & \dots & Y_{2,NS} \\ \vdots & \vdots & \ddots & \vdots \\ T_N & Y_{N,1} & \dots & Y_{N,NS} \end{bmatrix}$$

$Y_{i,j}$  = mass fraction of species  $j$  in cell  $i$

normalization

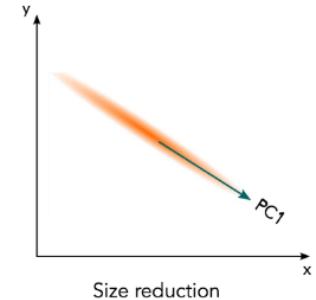
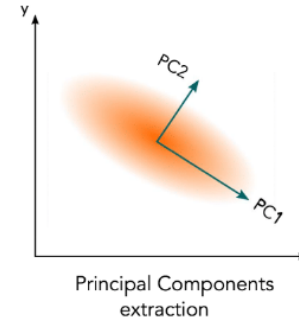
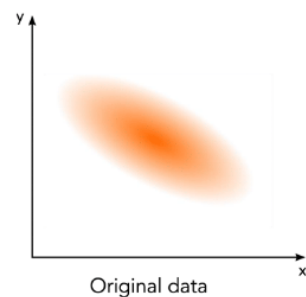
PCA

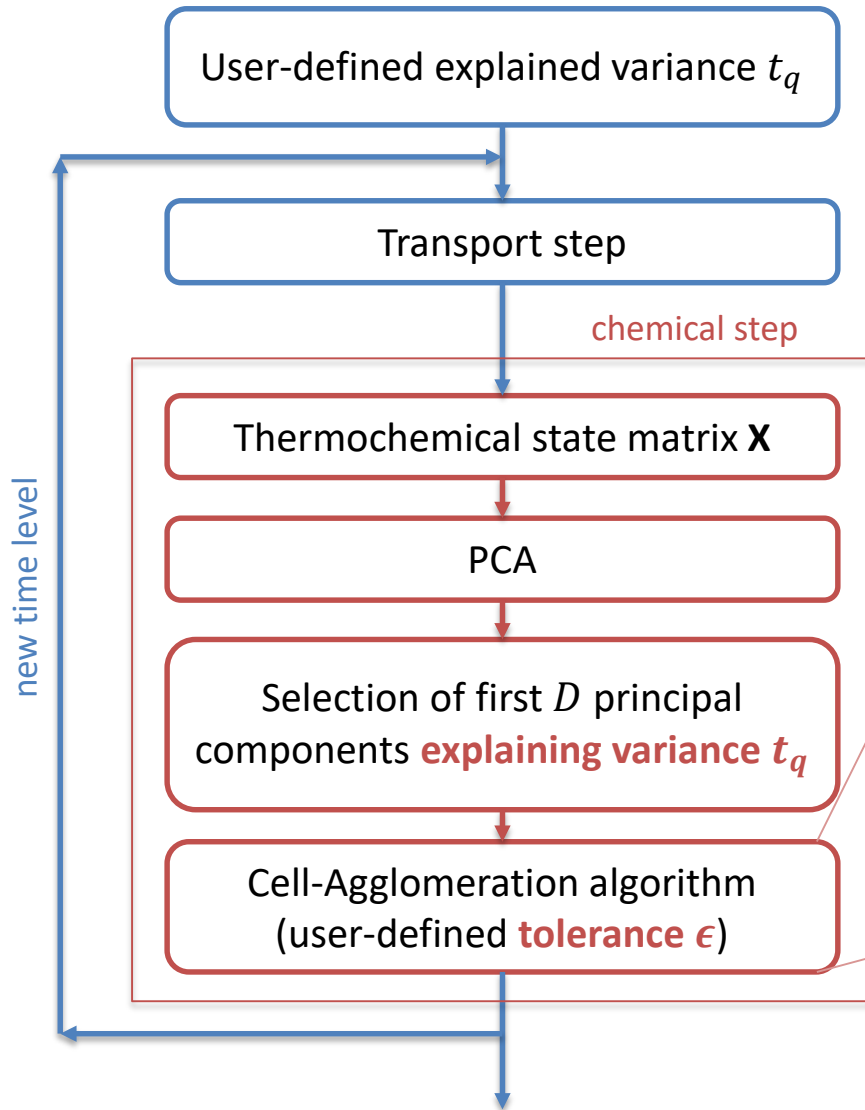
Principal  
Components

eigenvectors obtained  
from the decomposition  
of the covariance matrix

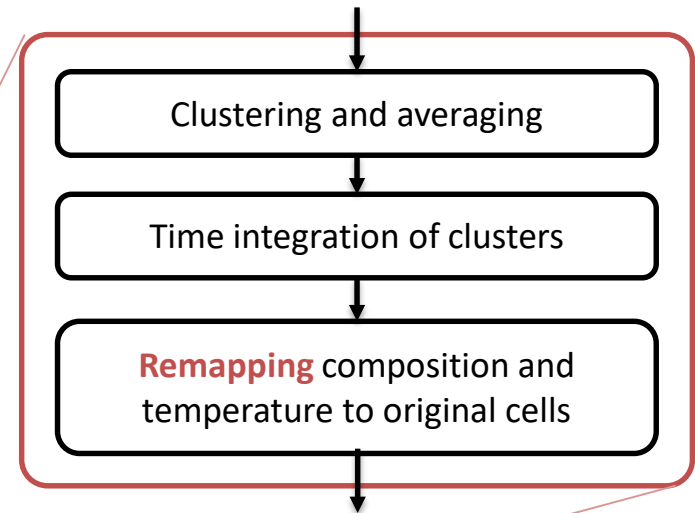
Input data matrix:  
 $N$  observations of  $NS + 1$  variables

$N$  = number of cells  
 $NS$  = number of species





By fixing  $t_q$ , the number  $D$  of principal components to be used is **automatically determined**.



F. Perini, R.D. Reitz, *Computationally efficient dimension reduction of combustion chemistry via Principal Components Analysis based domain partitioning*, Frontiers in Computational Physics: Energy Sciences Zurich, Switzerland June 5, 2015

## ISF F3 flames

Internal diameter: 4 mm

Velocities: 35 cm/s

Fuel composition: 80% C<sub>2</sub>H<sub>4</sub> + 20% N<sub>2</sub>

## Artificially imposed sinusoidal fluctuations of fuel stream velocity

Amplitude: 90%, Frequency: 10 Hz

## Kinetic mechanism

224 species and 5980 reactions

NO<sub>x</sub> chemistry included

<https://creckmodeling.chem.polimi.it>

## Computational domain

2D region (55 x 120 mm)

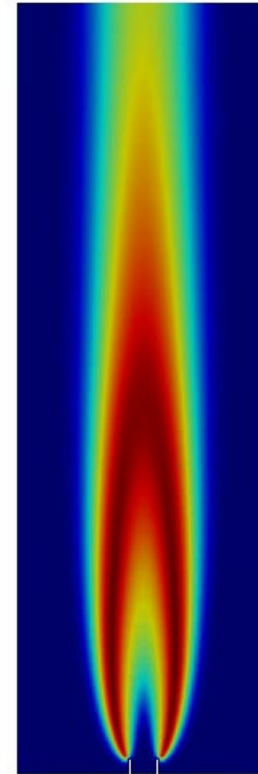
~25,000 cells

## Solver

laminarSMOKE++ (based on OpenFOAM 10)

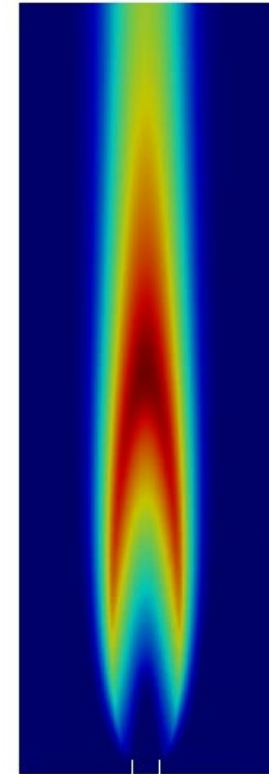
<https://github.com/acuoci/laminarSMOKE>

Temperature



300 K 2140 K

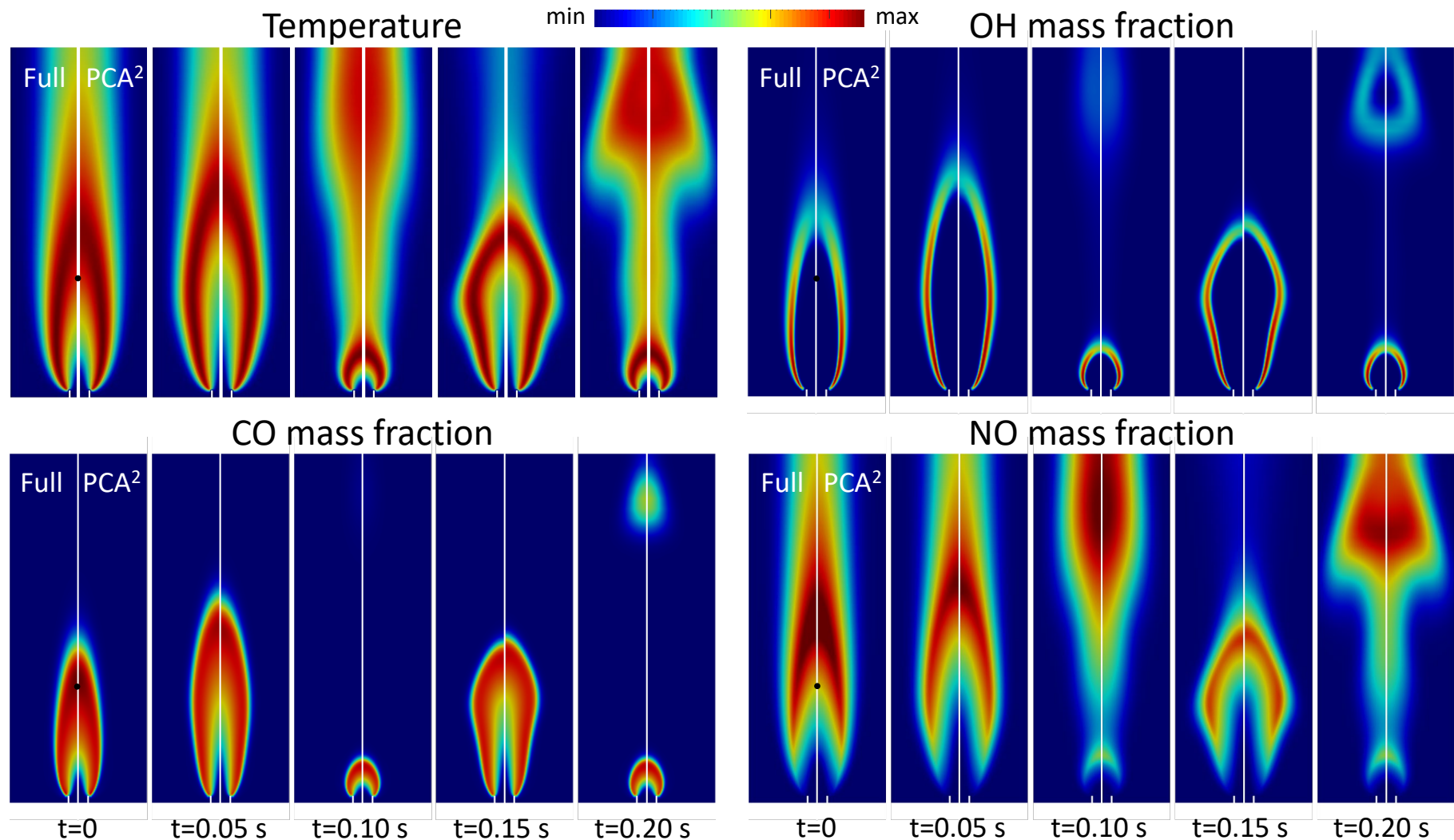
NO



0 10<sup>-4</sup>  
mass fraction

Smooke M.D., Long M.B., Connelly B.C., Colket M.B., Hall R.J.,  
Combustion and Flame, 143(4), p. 613-628 (2005)

# Example: $t_q = 50\%$ and $\epsilon = 0.010$

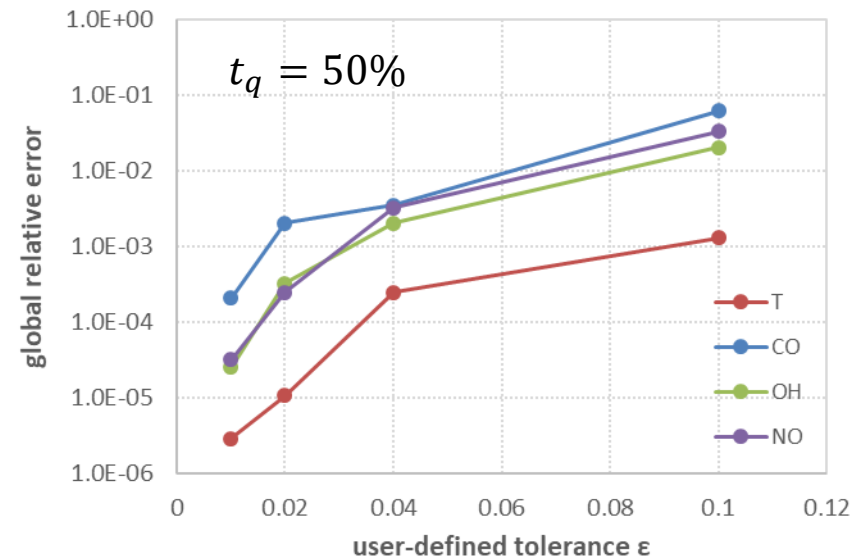
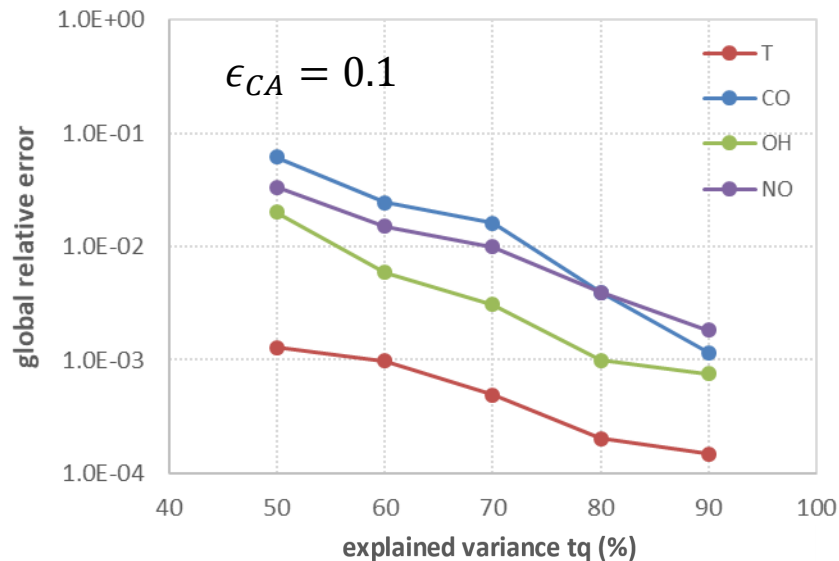


<https://www.kaggle.com/datasets/albertocuoci/laminar-coflow-flame-isf-f3a-pulsating>



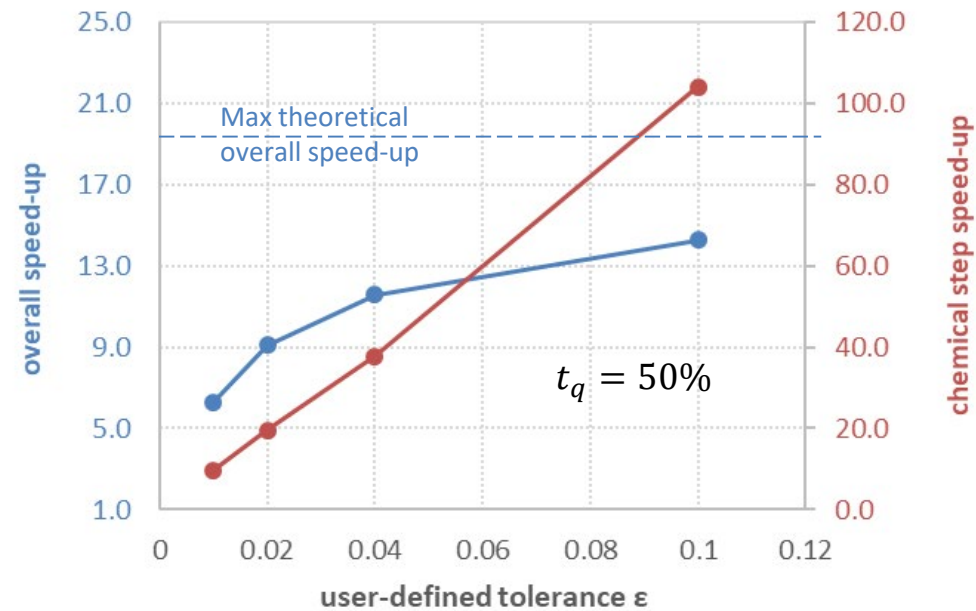
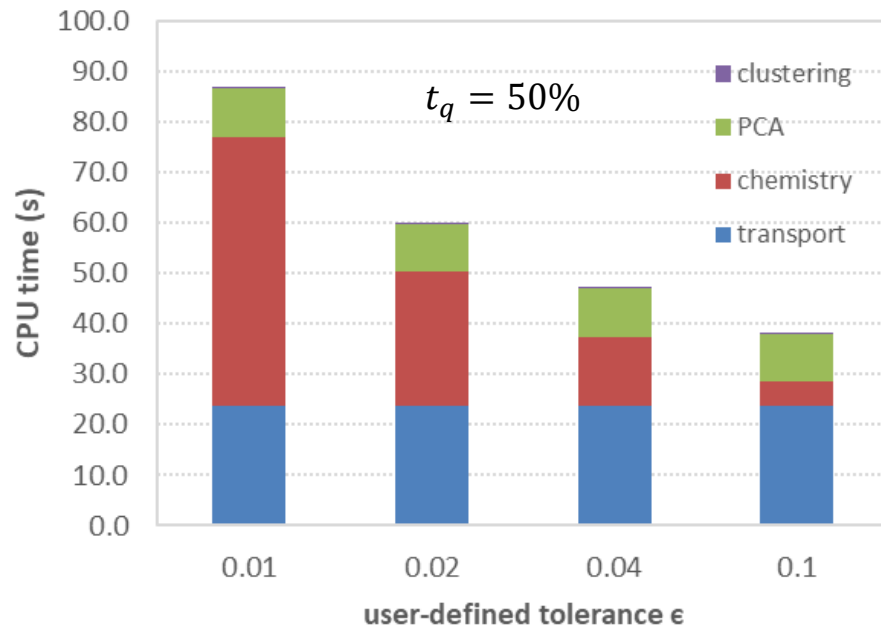
## User-defined parameters

- 1) Explained level of variance:  $t_q$
- 2) CA (Cell Agglomeration) tolerance:  $\epsilon_{CA}$



## CRECK PAH mechanism (224 species)

Chemistry CPU time: ~95%



## 1. $P(CA)^2$ : PCA-based Cell Agglomeration $P(CA)^2$

- Dynamic Cell Agglomeration and PCA
- Pulsating laminar coflow flame



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## 2. Tabulation-based SPARC-CA

- Temporally-evolving planar jet-flame
- 2D turbulent non-premixed flame including soot chemistry

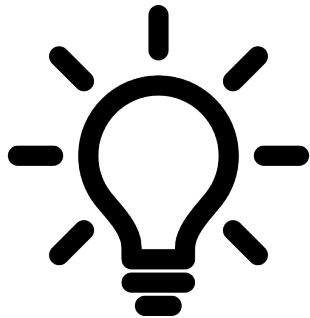




## (Dynamic) Adaptive Reduced Chemistry (ARC)

The **computational overhead** needed for the on-the-fly reduction of the mechanism can be significant, strongly reducing the efficiency of DAC

## Pre-partitioning



- A **library of reduced mechanisms** is built in a pre-processing step, covering the composition space which is expected to be visited by the reactive systems of interest.
- During the CFD simulation, before carrying out the chemical step, **each cell is classified**, i.e., the reduced mechanism available in the library is identified “instantaneously” and applied

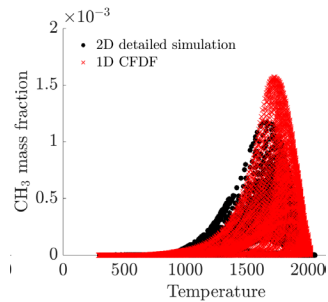
D.A. Schwer, P. Lu, and W.H. Green, Combustion and Flame, 133(4):451-465, 2003

Y. Liang, S.B. Pope, and P. Pepiot, Combustion and Flame, 162(9), 2015

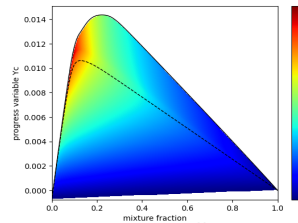
D'Alessio G., Parente A., Stagni A., Cuoci A., Combustion and Flame, 211, p. 68-82, 2020



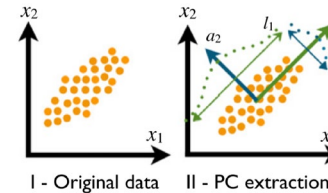
## 1. Pre-processing phase (SPARC)



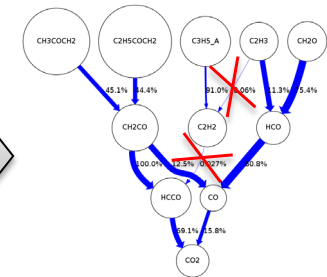
Dataset  
generation



Dataset re-mapping  
(or off-line classification)

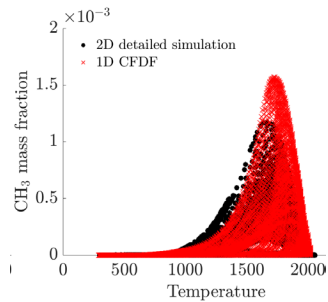


Partitioning

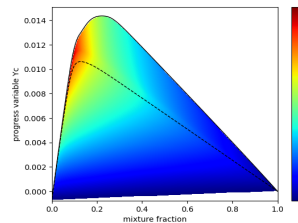


Reduced  
mechanisms

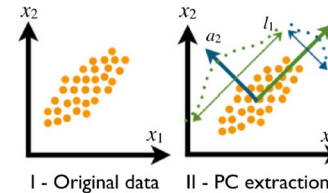
## 1. Pre-processing phase (SPARC)



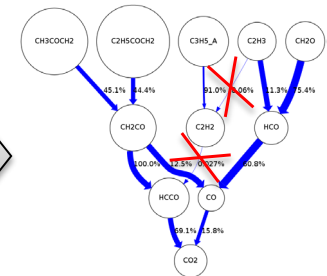
Dataset generation



Dataset re-mapping (or off-line classification)

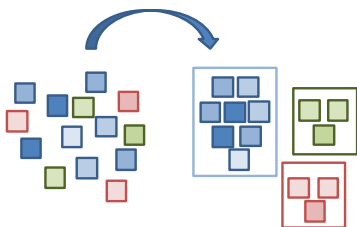


Partitioning

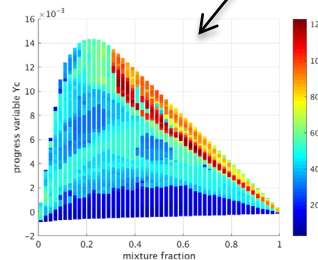


Reduced mechanisms

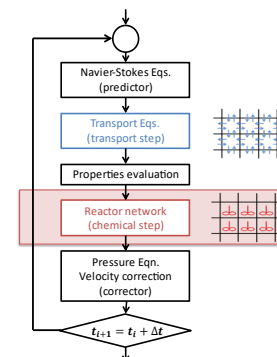
## 2. CFD simulation phase (CA)



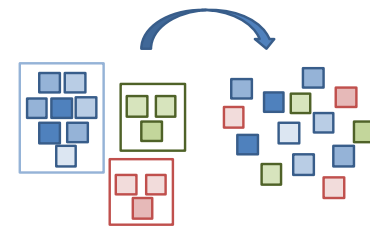
Cell agglomeration (CA)



On-the-fly classification



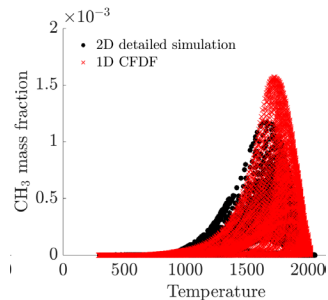
Numerical integration



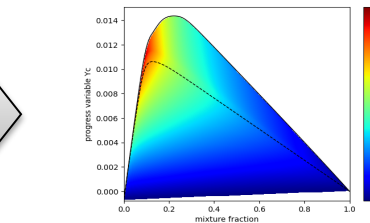
Back-mapping

## 1. Pre-processing phase (SPARC)

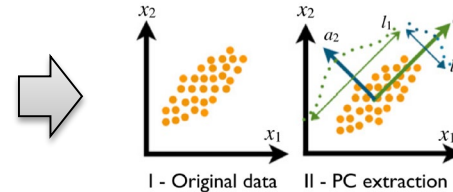
Kinetic Reduction  
tolerance  $\epsilon_{DRG}$



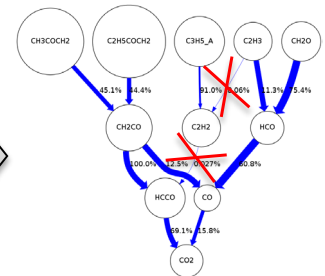
Dataset  
generation



Dataset re-mapping  
(or off-line classification)



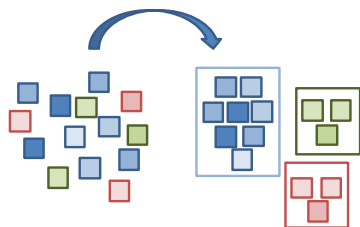
Partitioning



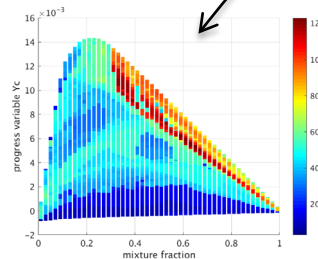
Reduced  
mechanisms

## 2. CFD simulation phase (CA)

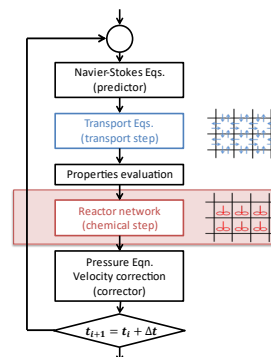
Cell Agglomeration  
tolerance  $\epsilon_{CA}$



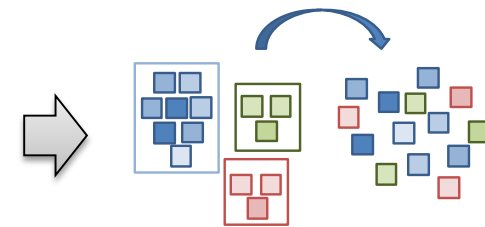
Cell agglomeration (CA)



On-the-fly  
classification

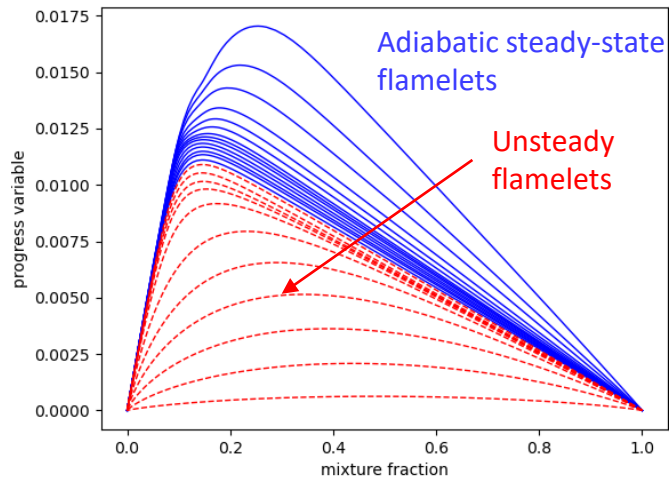


Numerical  
integration



Back-mapping

Fuel: C<sub>2</sub>H<sub>4</sub>/N<sub>2</sub> 0.90/0.10

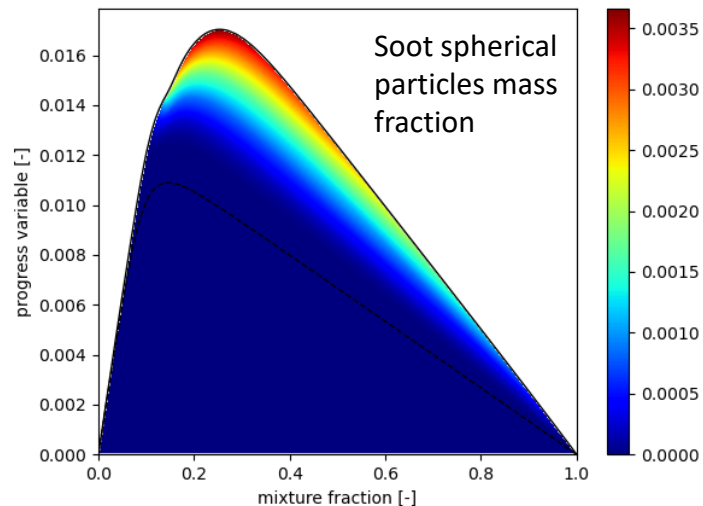


## Dataset generation

the training dataset is constructed from steady and unsteady adiabatic diffusion **flamelets**

## Dataset re-mapping

the generated database is re-mapped over two control variables, the **mixture fraction**  $\xi$  and the **progress variable**  $Y_C$

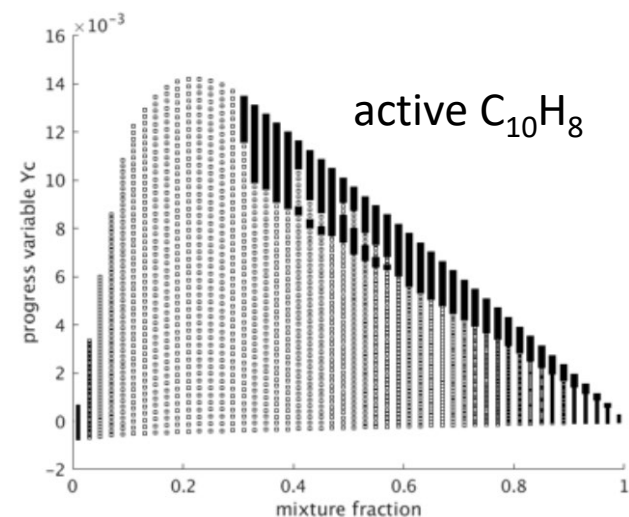
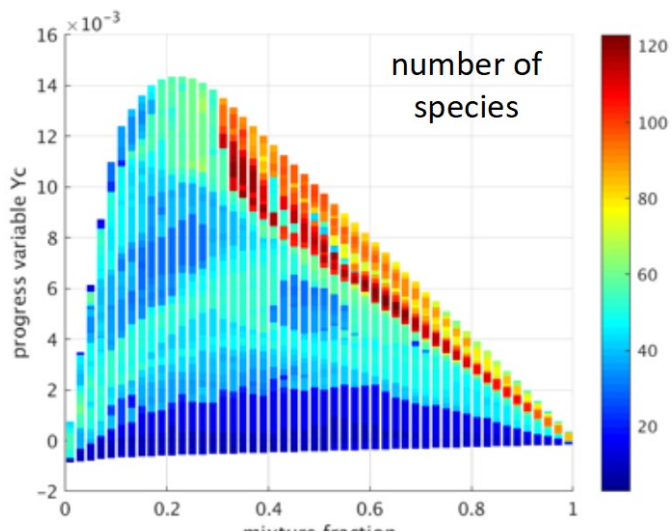


$$Y_C = \alpha_{CO_2} X_{CO_2} + \alpha_{H_2O} X_{H_2O} + \alpha_{CO} X_{CO} + \dots$$

Example of lookup table generated using a detailed kinetic mechanism including the soot chemistry via a Discrete Sectional Method (DSM)



Original mechanism:  
226 species, ~10,400 reactions



## Partitioning

A **clustering algorithm** in the  $\xi - Y_c$  space is adopted to identify continuous regions (i.e., clusters) having similar kinetic behavior

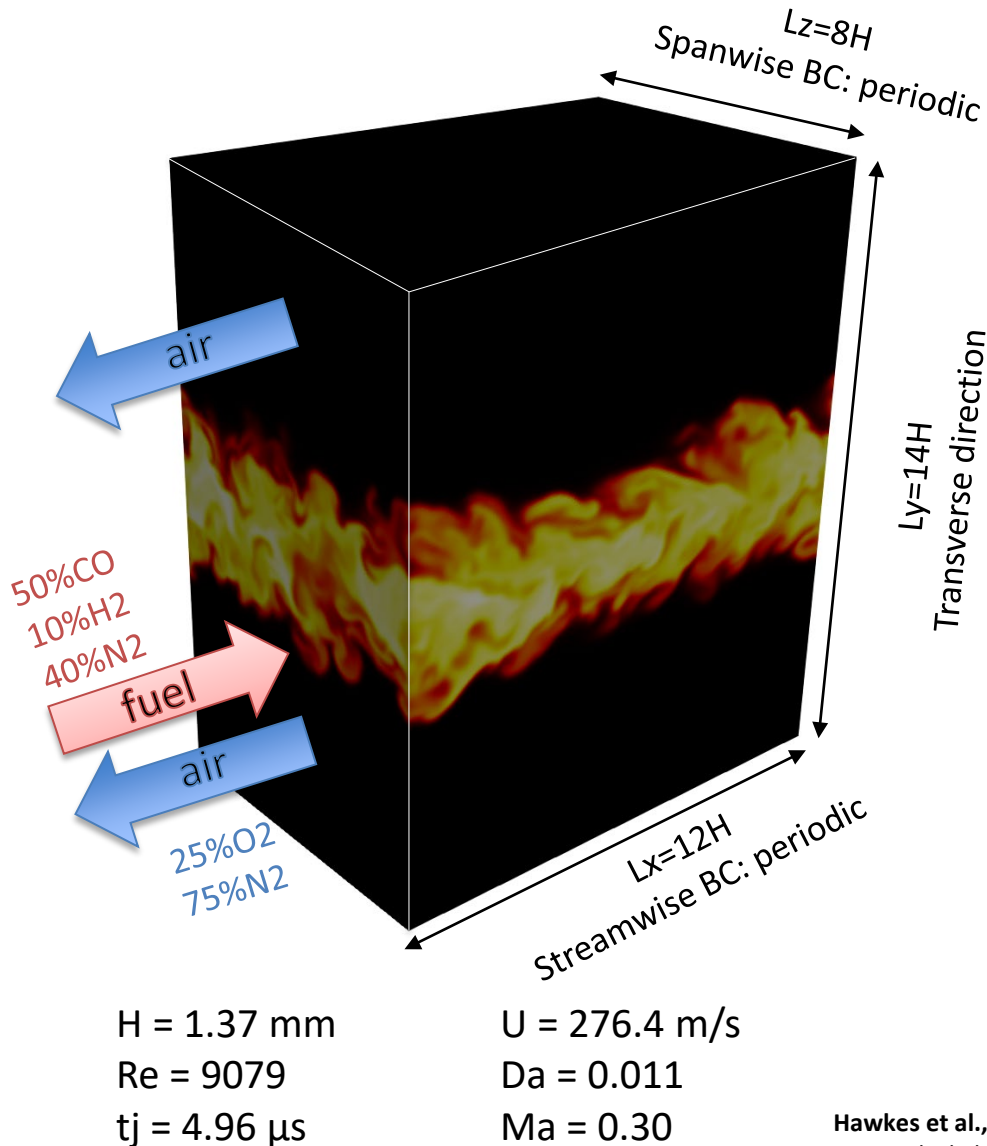
Surapaneni A., Mira D., Combustion and Flame 251:112715 (2023)

## Generation of reduced mechanisms

For each cluster of the dataset, a reduced mechanism is generated via the **Directed Relation Graph (DRG)** method

P. Pepiot-Desjardins, H. Pitsch, Combustion Theory and Modelling 12, 1089-1108 (2008)

# Temporally-evolving planar jet-flame



## 2D Mesh

$\Delta x = 30 \mu\text{m}$  or  $45 \mu\text{m}$   
Mesh:  $548 \times 640$  or  $365 \times 426$   
Cells:  $\sim 350\text{k}$  or  $\sim 156\text{k}$

## Quasi-DNS (3D)

$\Delta x = 90 \mu\text{m}$   
Mesh:  $182 \times 214 \times 122$   
Cells:  $\sim 4.75\text{M}$

## Kinetic mechanisms

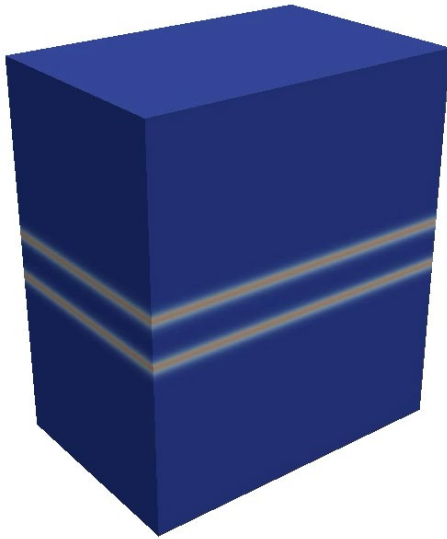
Detailed H<sub>2</sub>/CO + NO<sub>x</sub> mechanism by **CRECK**:  
57 species and 385 reactions

<https://creckmodeling.chem.polimi.it>

## Solver

laminarSMOKE++ (based on OF-10)  
Time discretization: 2nd order backward Euler  
Space discretization: OF *cubic* scheme

Hawkes et al., Scalar mixing in direct numerical simulations of temporally evolving plane jet flames with skeletal CO/H<sub>2</sub> kinetics, Proceedings of the Combustion Institute, 31, p. 1633-1640 (2007)

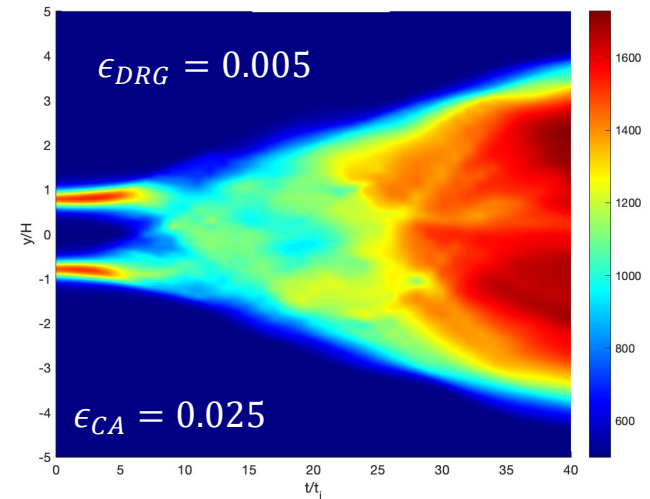
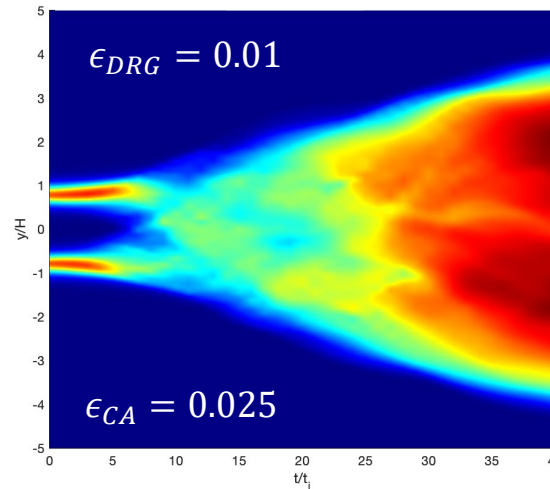
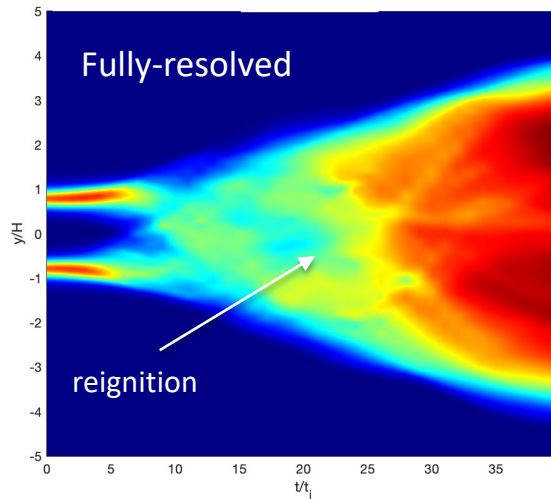


Relevant fields (temperature and mass fractions of species) are **spatially-averaged** over x-z planes

$$\varepsilon = \frac{1}{N_Y N_T} \sum_{k=1}^{N_T} \sum_{i=1}^{N_Y} \frac{|\psi_{k,i}^{CA} - \psi_{k,i}|}{\psi_{max}}$$

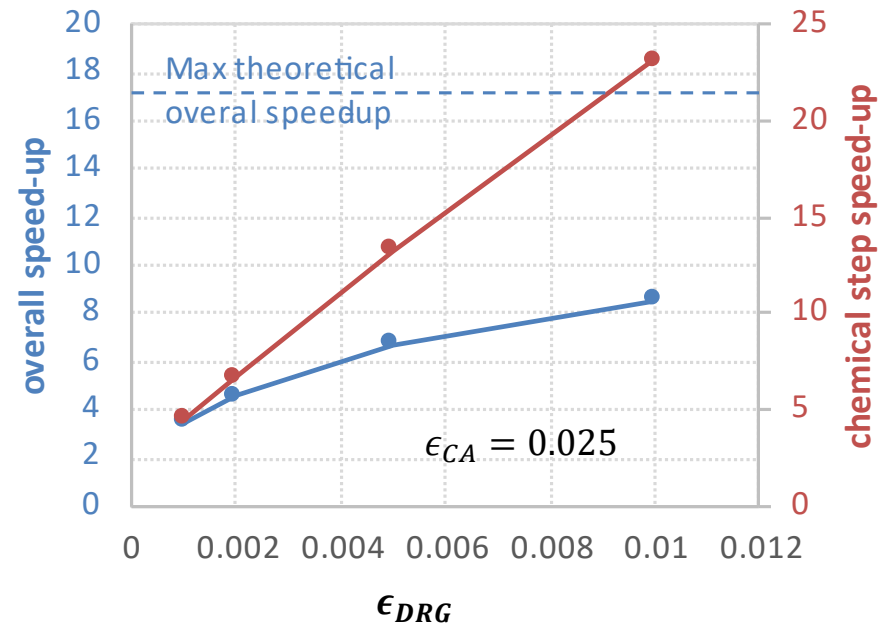
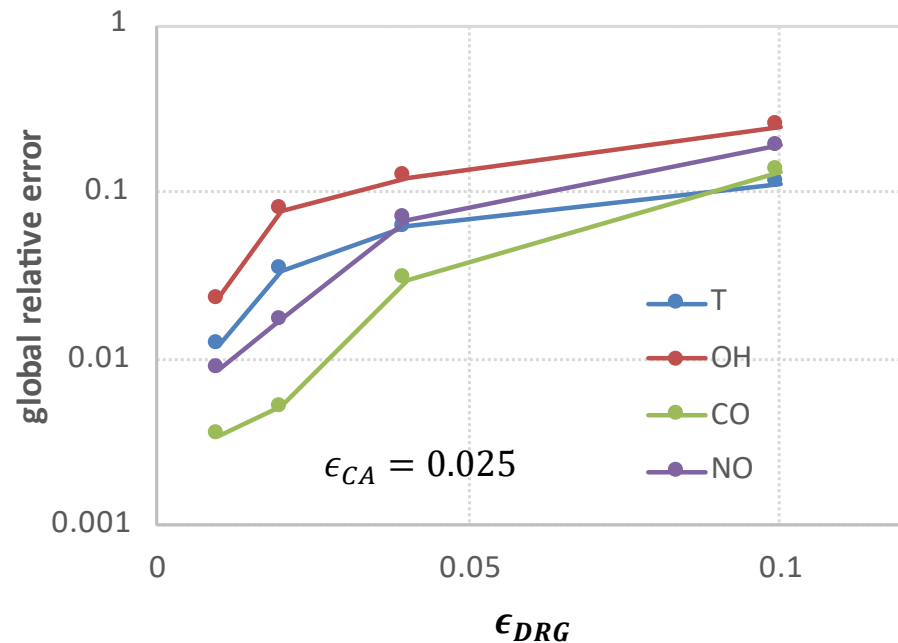
$\psi_{k,i}$  spatially-averaged fully-resolved solution at  $y_i$  at time  $k$

$\psi_{k,i}^{CA}$  spatially averaged CA-based solution at  $y_i$  at time  $k$

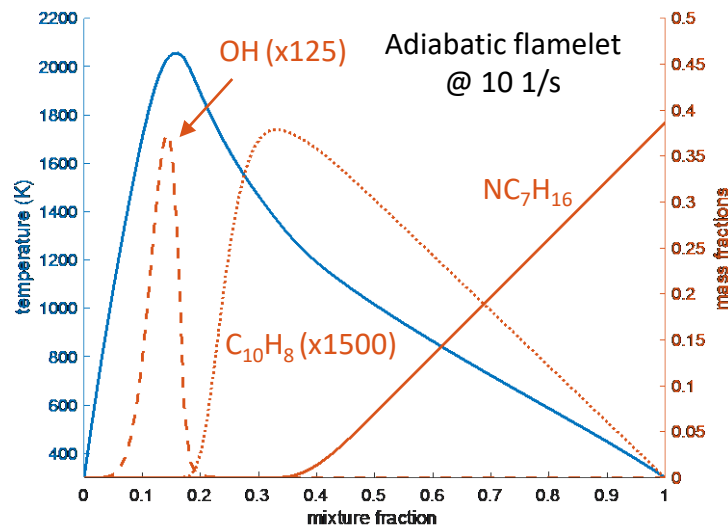
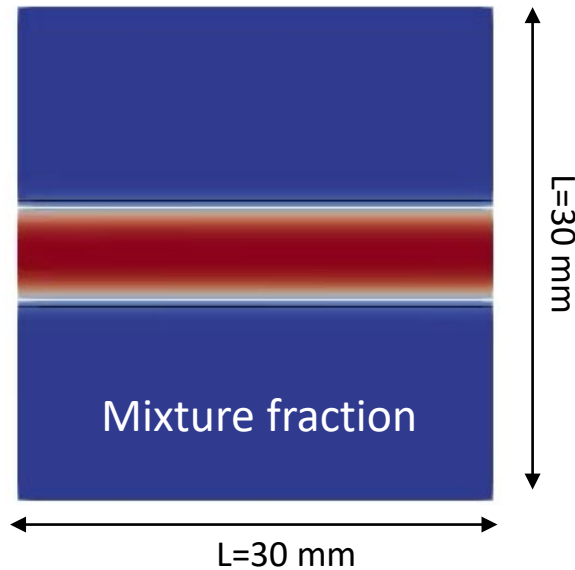


## CRECK2003-NOX mechanism (57 species)

Chemistry CPU time: 93%



# 2D turbulent non-premixed flame



## Quasi-DNS (2D Mesh)

$\Delta x = 75 \mu\text{m}$

Mesh: 400 x 400

Cells: 160k

Simulation time: 30 ms (max Courant number: 0.2)

Boundary conditions: periodic

## Kinetic mechanism

CRECK HT-PRF + Soot (**Discrete Sectional Method**):

226 (pseudo-)species, ~10,400 reactions

## Numerical details

Solver: laminarSMOKE++ (based on OF-10)

Time discretization: 2nd order backward Euler

Space discretization: OF *cubic* scheme

## Operating conditions

Fuel: 84.4% NC7H16 + 15.6% N2

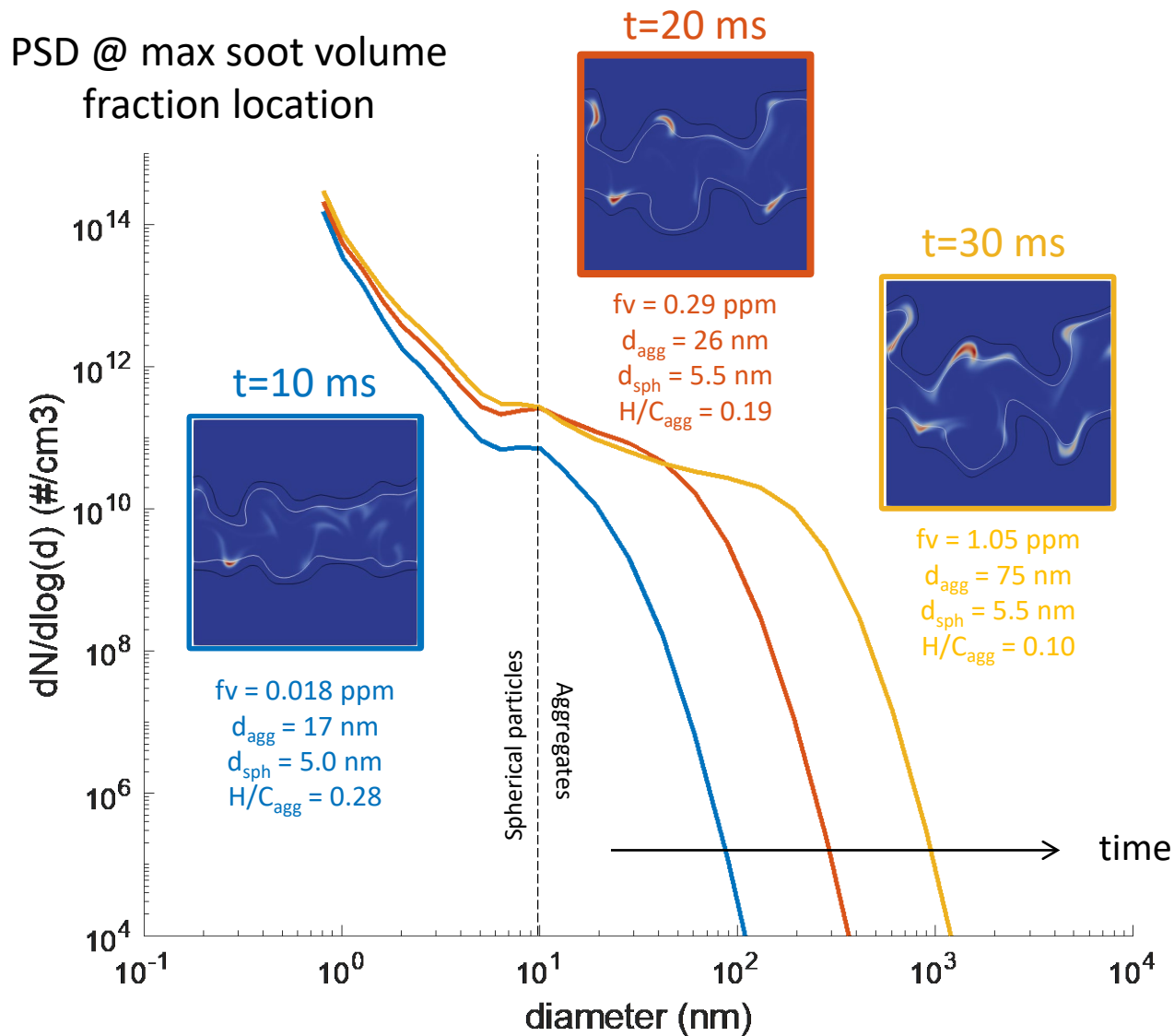
Oxidizer: 21% O2 + 79% N2

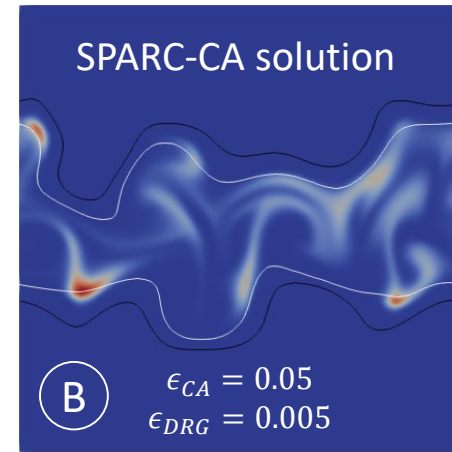
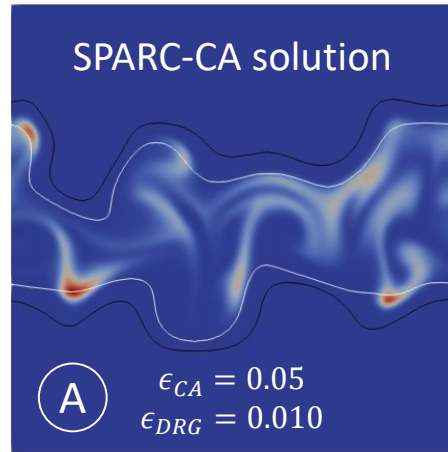
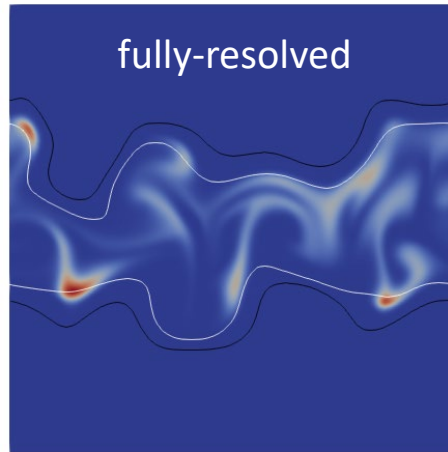
Initial temperature: 300 K

Initial pressure: 1 atm

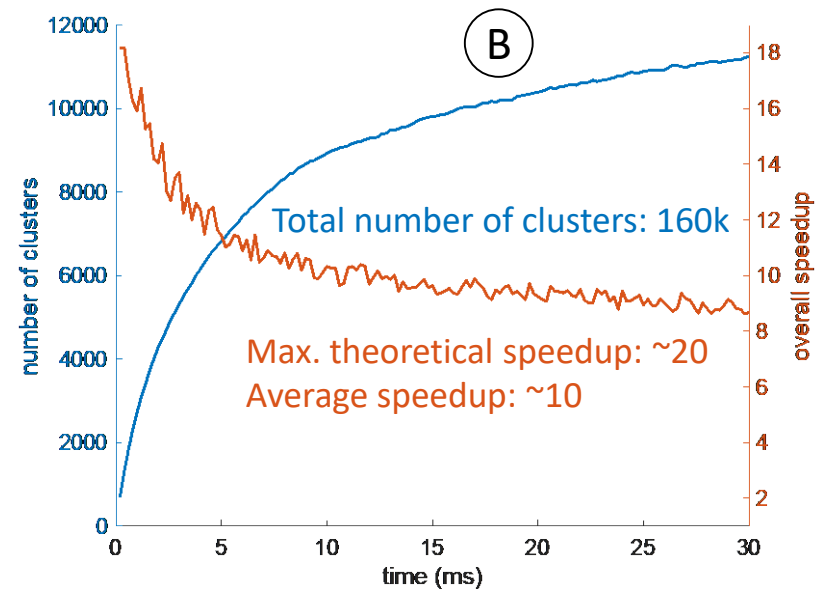
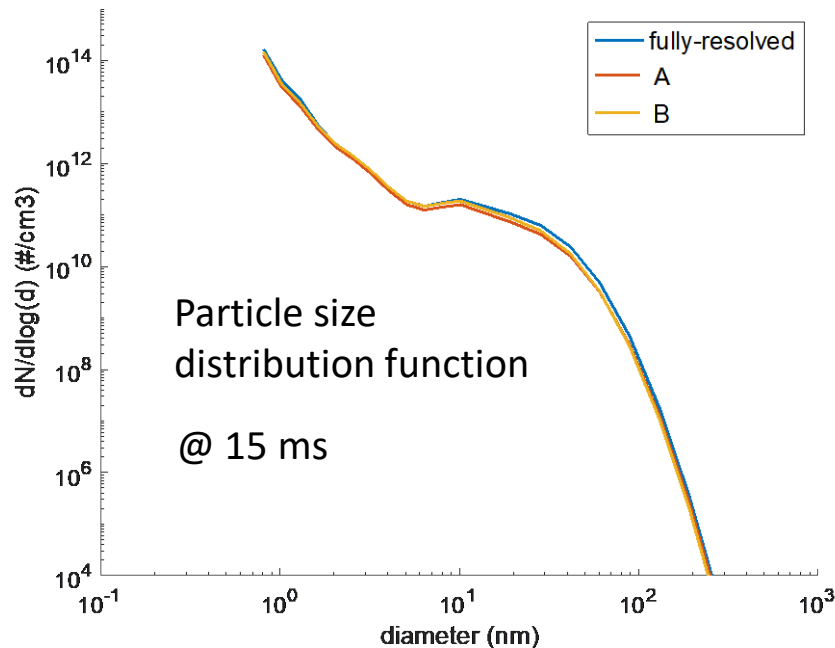
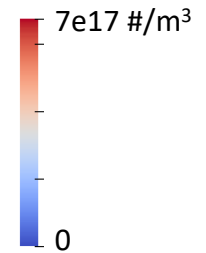
Bisetti et al., On the formation and early evolution of soot in turbulent nonpremixed flames, Combustion and Flame, 159, p. 317-335 (2012)

# Particle Size Distribution (PSD) of soot





Soot particle  
number density  
@ 15 ms





## 1. Reducing the number of cells: $P(CA)^2$

- Combination of Cell Agglomeration and PCA
- Optimal/automatic choice of features for cell agglomeration

## 2. ... and reducing the kinetic complexity: Tabulation-based SPARC-CA

- Combination of Adaptive Reduced Chemistry (ARC) and Cell-Agglomeration
- Chemical reduction as a preprocessing step

# Acknowledgements



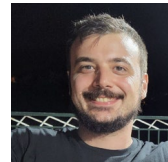
<http://creckmodeling.chem.polimi.it>



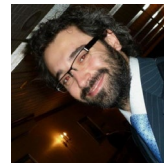
Heinz  
Pitsch



Alessandro  
Parente



Giuseppe  
D'Alessio



Temistocle  
Grenge



**Alexander von Humboldt**  
Stiftung / Foundation

Part of this work was  
supported by the  
**Alexander von Humboldt**  
Foundation

# Thank you!



## ... and see you in Milan in July 2024!

<http://www.combustionsymposia.org/2024/>



# Thank you!

CRECK Modeling Group  
Department of Chemistry, Materials  
and Chemical Engineering “G. Natta”  
[creckmodeling.chem.polimi.it](http://creckmodeling.chem.polimi.it)

Follow us on Social Media  
@CreckModeling



**... and see you in Milan in 2024!**

<http://www.combustionsymposia.org/2024/>

## OpenSMOKE++

<https://www.opensmokepp.polimi.it>

Thermodynamics and detailed kinetics  
Multicomponent transport properties  
ODE solvers for stiff chemistry  
Tools for kinetic analysis (ROPA)

- **Ideal reactors** (batch, PFR, CSTR, shock-tubes, RCM)
- **Laminar 1D flames** (burner stabilized, freely propagating, counter-flow flames)
- Isolated fuel droplets
- Steady-state laminar flamelets
- Heterogeneous catalytic ideal reactors (batch, PFR, CSTR)

Cuoci A. et al., Computer Physics Communications, 192, pp. 237-264, DOI: [10.1016/j.cpc.2015.02.014](https://doi.org/10.1016/j.cpc.2015.02.014)

Cuoci A. et al. (2013) Combustion and Flame, 160 (5), pp. 870-886, DOI: [10.1016/j.combustflame.2013.01.011](https://doi.org/10.1016/j.combustflame.2013.01.011)

## OpenFOAM-based Codes

laminarSMOKE++  GitHub

- CFD of laminar reacting flows (coflow flames, burner stabilized stagnation flames, ...)

flameletSMOKE++  GitHub

- Turbulent flames based on the steady-state laminar flamelet

edcSMOKE++   GitHub

- Turbulent flames based on the Eddy Dissipation Concept (EDC) model

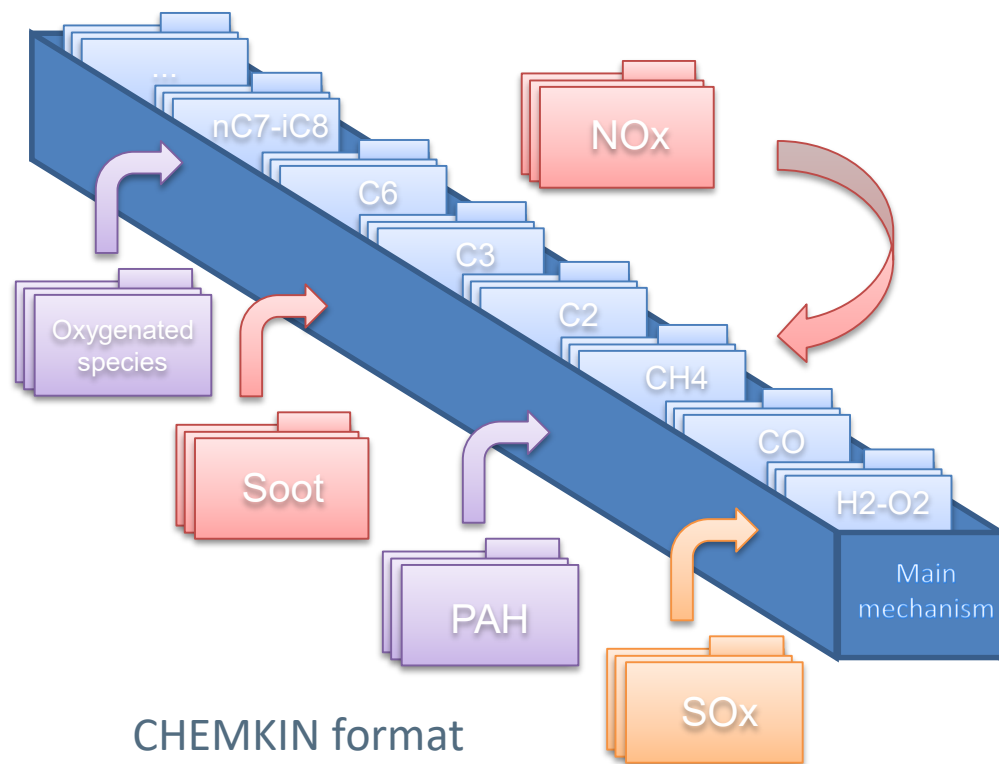
catalyticFOAM\*



- Simulation of catalytic heterogeneous (gas/solid) reactors

\* In cooperation with M. Maestri (POLIMI)





Kinetic mechanism of **pyrolysis, oxidation and combustion** of small (C1-C3) and large hydrocarbons up to Diesel and jet fuels (C16) as well as several pollutants

**Hierarchy**

**Modularity**

**Generality**

~ 600 chemical species

~ 20,000 reactions

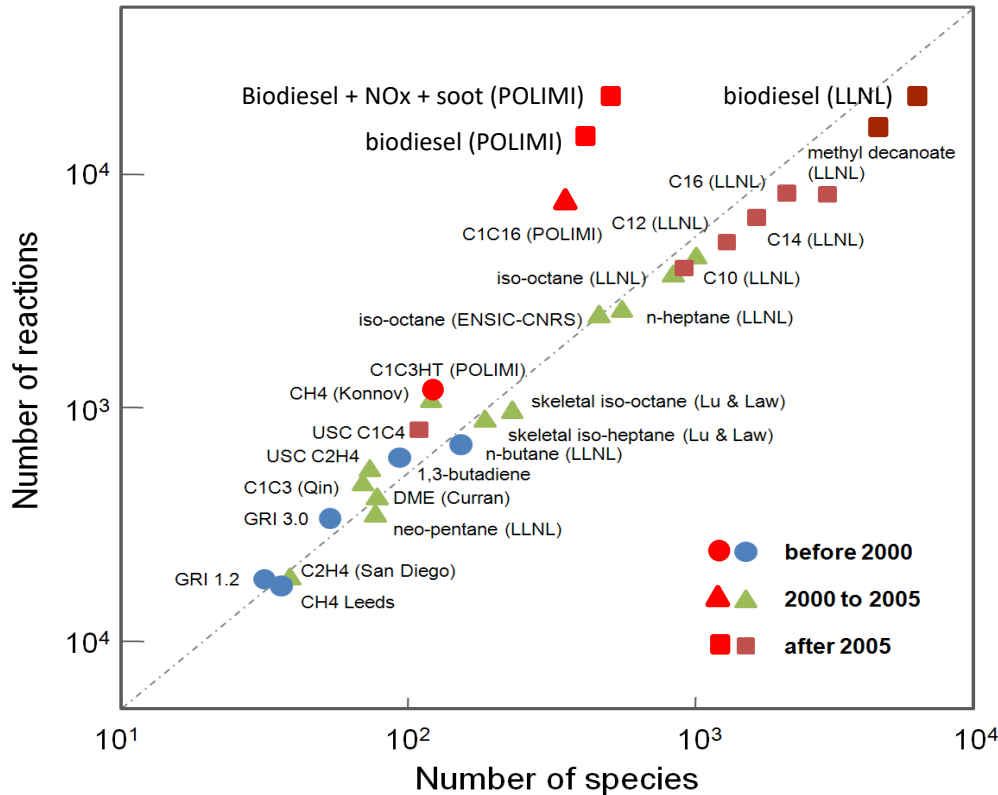
<http://creckmodeling.chem.polimi.it>

Frassoldati, A. et al., Combustion and Flame 157(2010), pp. 2-16 [\[Link\]](#)

Ranzi, E. et al., Progress in Energy and Combustion Science 38 (2012), pp. 468-501 [\[Link\]](#)







Adapted from: **T.F. Lu, C.K. Law**, *Toward accommodating realistic fuel chemistry in large-scale computations*, Progress in Energy and Combustion Science, 35, p. 192–215 (2009)

need of **numerical techniques** and **computational tools** to make:

- the use of large kinetic mechanisms computationally efficient
- their **integration** in new and/or existing numerical codes as smooth as possible

## 1. Number of equations

Detailed kinetic mechanisms may involve dozens or **hundreds** of chemical species

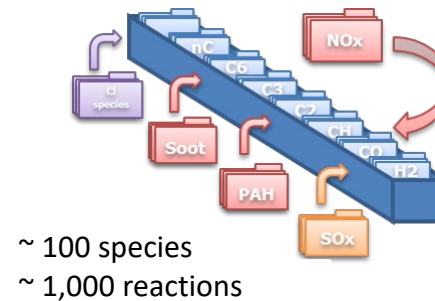
## 2. Non-linearity and coupling

The transport equations of species and energy are very **non-linear and strongly coupled**

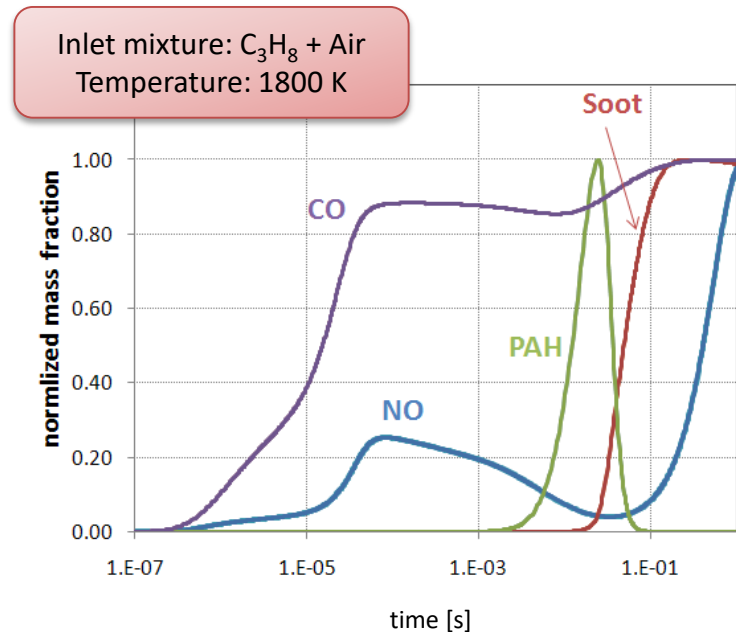
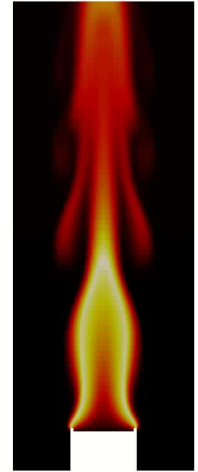
## 3. Stiffness

The **characteristic times** of species involved in a kinetic scheme can differ by several order of magnitudes

### Detailed kinetic mechanisms



Unsteady flame

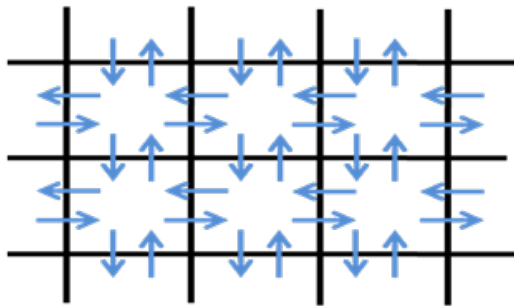


$$\frac{d\mathbf{Y}}{dt} = \mathbf{T} + \mathbf{S}$$

Transport  
(convection + diffusion)  
Chemistry  
(reactions)

$$\begin{cases} \Delta \mathbf{Y}_1^n = \Delta t \mathbf{T}^n \\ \Delta \mathbf{Y}_2^n = \Delta t \mathbf{S}^n \end{cases}$$

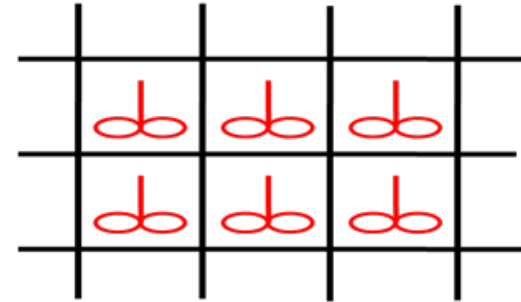
Transport step ( $\Delta t$ )



$$\frac{d\mathbf{Y}}{dt} = \mathbf{T}$$



Chemical step ( $\Delta t$ )



$$\frac{d\mathbf{Y}}{dt} = \mathbf{S}$$

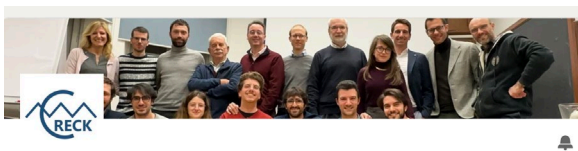
**Strang G.**, *On the construction and comparison of difference schemes.* SIAM Journal of Numerical Analysis, 5, p. 506-517 (1968)

**Ren Z., Pope S.B.**, *Second-order splitting schemes for a class of reactive systems.* Journal of Computational Physics, 227 p. 8165-8176 (2008)

## The CRECK Modeling Lab is recruiting PhD Students and Postdocs

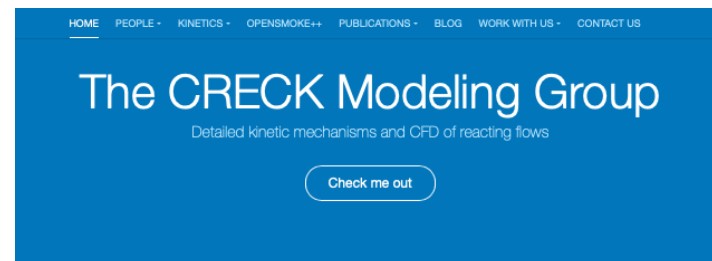
- Numerical modeling of **reactive flows** with detailed kinetics
- Development of **detailed kinetic mechanisms** for pyrolysis, oxidation and combustion of gaseous fuels
- Theoretical calculation of **rate constants** in gas-phase and heterogeneous phase
- Modeling of volatilization, gasification and combustion of **biomasses**
- Modeling of thermal conversion (gasification/pyrolysis) of **plastics**
- CFD and compartment-based modeling of **bioreactors**

We are open to possible collaborations on the same topics!



CRECK Modeling

Chemical Reaction Engineering || Chemical Kinetics || CFD simulations of reacting flows || Based



### Team members



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The Chemical Reaction Engineering and Chemical Kinetics Lab has a consolidated experience in the development of detailed and semi-detailed kinetic mechanisms of the pyrolysis, oxidation and combustion of gas, liquid and solids. The group is led by Prof. Tiziano Faravelli and includes 2 full professors, 2 associate professors, 2 assistant professors, 1 post doctoral researcher and 4 PhD students.



### Detailed kinetic mechanisms

Detailed kinetic models constitute a very useful tool for the proper understanding of combustion processes and the characterization of typical phenomena like ignition delays and induction times, flame structure and pollutant formation. Design, simulation, optimization and control of industrial burners, gas turbines, boilers, incinerators and gasifier are typical application, as well as the design of internal combustion engines and the formulation of new fuels. The CRECK Lab has a consolidated experience of the development of detailed and semi-detailed kinetic mechanisms of the pyrolysis, oxidation and combustion of gas, liquid and solids.

### CFD of flames with detailed chemistry

Combustion devices (domestic and industrial burners, furnaces, internal combustion engines, combustors for automobiles, etc.) have to respect always more stringent limitations concerning the emissions of pollutant species, like CO, NO<sub>x</sub>, PAHs, soot, etc. Computational fluid dynamics (CFD), coupled with detailed kinetic mechanisms, represents a fundamental tool to study such devices and to characterize them in terms of formation of pollutants. This paves the route towards a more rational design, based on predictive numerical models.

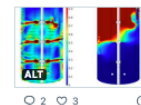
### Solid fuels

The environmental concerns towards the combustion of fossil fuels drive the interest in gasification processes of biomasses, plastics, wastes and refuse derived fuels (RDF). Gasification of solid fuels is nowadays a promising alternative to direct combustion, both electric and thermal energy are viable products, together with chemicals. The low costs and the availability of raw materials, combined with its renewability in the biomass scenario, justify the interest in this technology. Nevertheless, the complexity of this

### Tweets from @CRECKLab



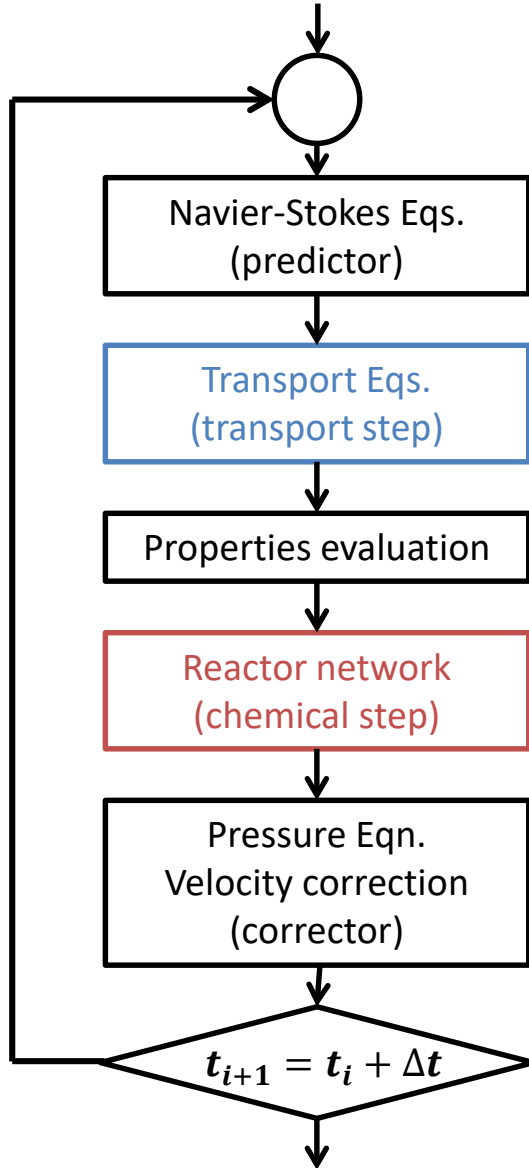
PHD position available in CRECK Lab on CFD of bubble column bioreactors for the production of bio-methane from renewable hydrogen in collaboration with @fiorentini3pal  
Read more: [creckmodeling.chem.polimi.it/blog/431-blog---@polimi\\_phdpositions](https://creckmodeling.chem.polimi.it/blog/431-blog---@polimi_phdpositions) #hydrogen #biomethane #phdposition #renewableenergy



New PhD position available in CRECK Lab on numerical modeling of Chemical Vapor Infiltration (CVI) for production of carbon disk brakes for racing cars in collaboration with @BremboBrakes! Read more: [creckmodeling.chem.polimi.it/blog/429-blog---@polimi\\_phdpositions](https://creckmodeling.chem.polimi.it/blog/429-blog---@polimi_phdpositions)



<http://creckmodeling.chem.polimi.it>



Chemical Step = **independent ODE systems** with IC

**Implicit ODE solvers** are mandatory!

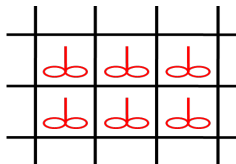
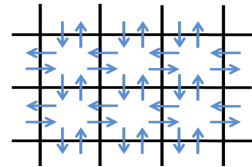
Implicit ODE solvers are **computationally very expensive**

The cost increases more than linearly with the number of species  $N_S$ :

$$cost \sim N_S^{2 \div 3}$$



**Need of acceleration techniques for speeding-up the chemical step**



Cuoci, A., Frassoldati, A., Faravelli, T., Ranzi, E., *Numerical modeling of laminar flames with detailed kinetics based on the operator-splitting method* (2013) *Energy and Fuels*, 27 (12), pp. 7730-7753

For each solver, a **C++ interface in OpenFOAM** was created

## 1. Creating ODE System objects

```
ODESystem_BatchReactor_DVODE *odeSystemObject;  
odeSystemObject = ODESystem_BatchReactor_DVODE::GetInstance();
```

## 2. Creating ODE System Solver

```
OpenSMOKE_DVODE<ODESystem_BatchReactor_DVODE> ode(odeSystemObject);
```

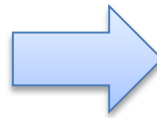
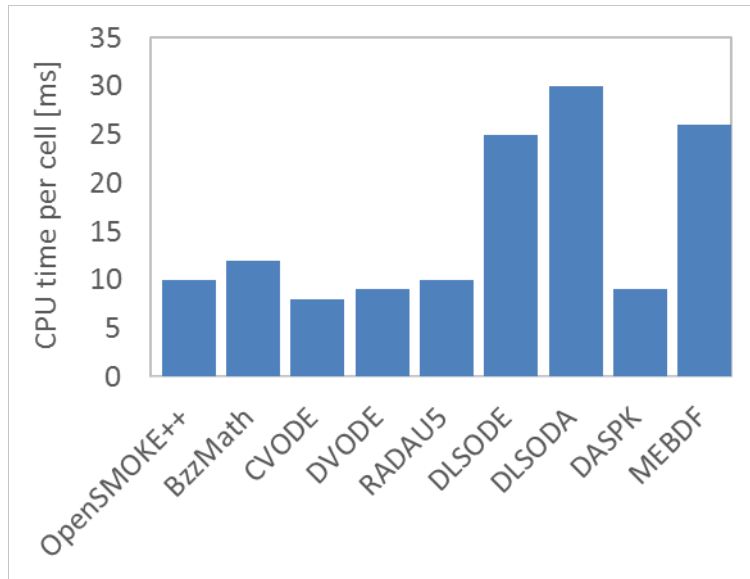
## 3. Setting numerical parameters

```
ode.SetMaximumNumberOfSteps(100000);  
ode.SetAnalyticalJacobian(false);  
ode.SetAbsoluteTolerance(aTol);  
ode.SetRelativeTolerance(rTol);
```

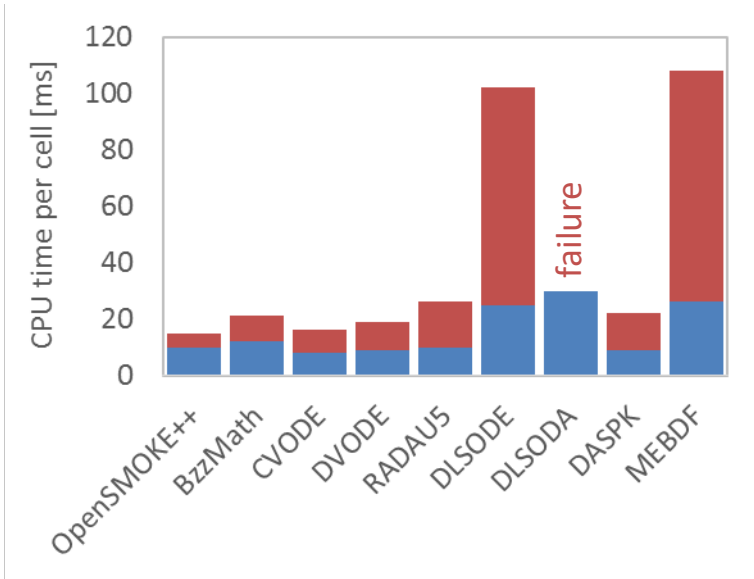
## 4. Looping on computational cell

```
ode.SetInitialValues(t0, Y0);  
ode.Solve(tf);  
ode.Solution(yF);
```

Homogeneous mechanism  
105 species, 1700 reactions



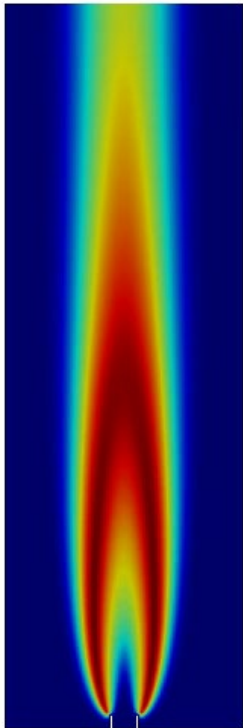
Addition of a heterogeneous mechanism  
12 species, 38 reactions



Micro-kinetic mechanisms for heterogeneous reactions are usually very non-linear because the activation energy may depend on the coverage (i.e., the composition on the catalytic wall)

$$r_j = A_j \cdot T^{\beta_j} \cdot \exp\left(-\frac{E_{att,j}(\theta_i)}{RT}\right) \prod_{i=1}^{NC} (c_i)^{v_{ij}}$$

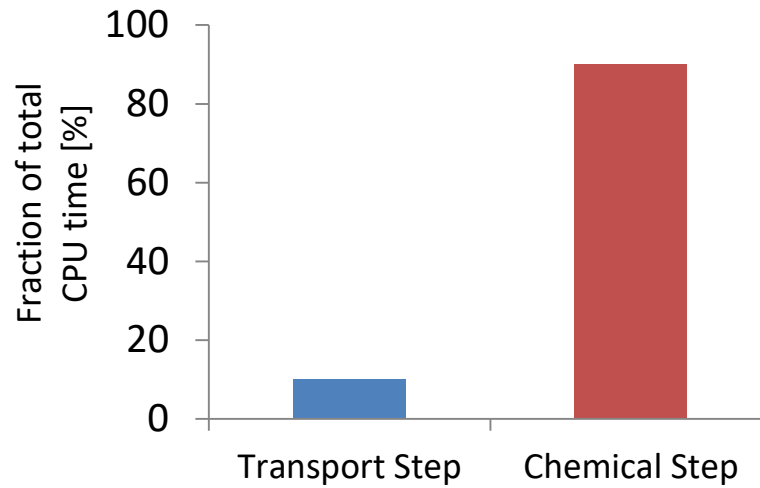




**Pulsating laminar coflow flame**

**Imposed sinusoidal fluctuations of fuel stream velocity**

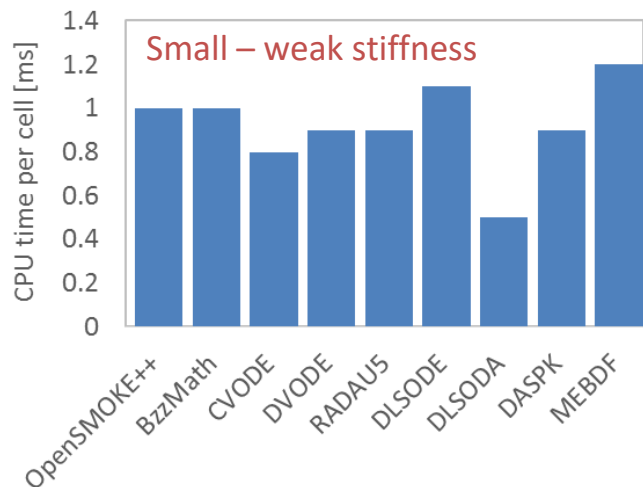
Amplitude: 90%  
Frequency: 10 Hz



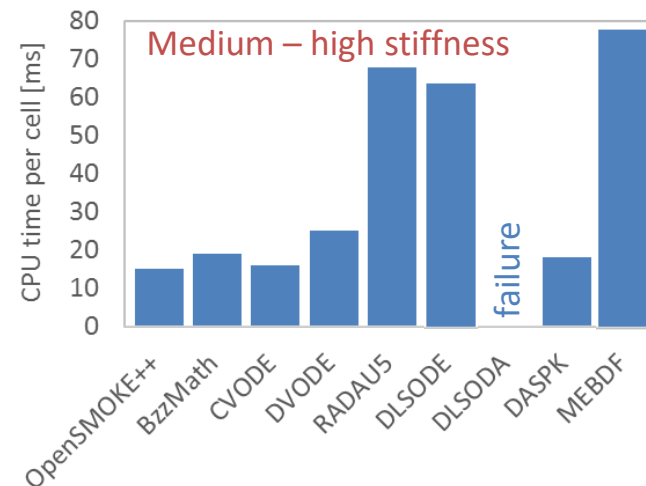
Most of the CPU Time (>90%) is spent for the numerical integration of the ODE systems corresponding to the chemical step

	Language	Code available	License
OpenSMOKE++	C++	Yes	Academic use only
BzzMath	C++	No	Academic use only
DVODE	FORTRAN	Yes	Free
CVODE	C	Yes	Free
DLSODE	FORTRAN	Yes	Free
DLSODA	FORTRAN	Yes	Free
RADAU5	FORTRAN	Yes	Free
DASPK	FORTRAN	Yes	Free
MEBDF	FORTRAN	Yes	Free

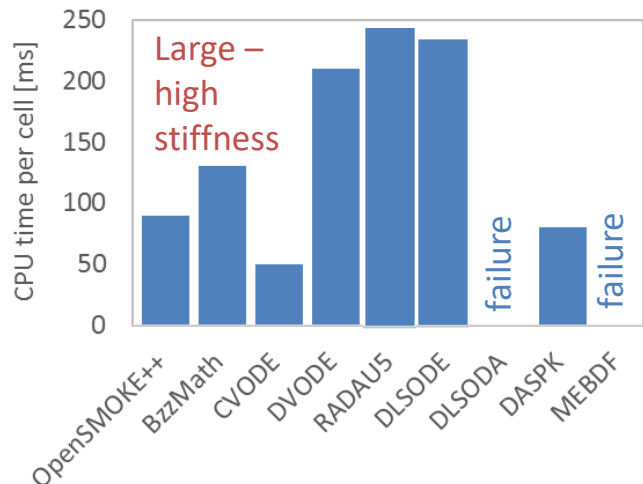
Homogeneous mechanism  
19 species, 140 reactions



Homogeneous mechanism  
156 species, 5400 reactions



Homogeneous mechanism  
680 species, 2400 reactions

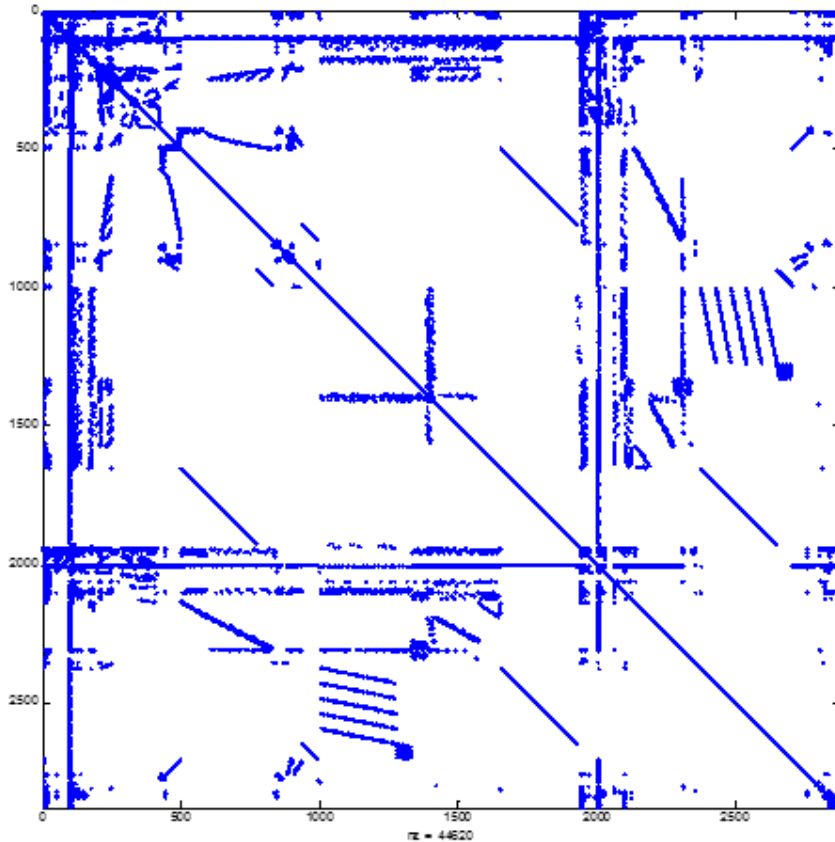


The best ODE solver depends on the features of the kinetic mechanism adopted:

- ✓ number of species
- ✓ species/reactions ratio
- ✓ lumped reactions

**Cuoci A. et al.**, *OpenSMOKE++: An object-oriented framework for the numerical modeling of reactive systems with detailed kinetic mechanisms* (2015) Computer Physics Communications, 192, pp. 237-264

## Jacobian sparsity pattern



LLNL methyl-decanoate

Species: 2878

Reactions: 8555

Non-zero elements: 44620 / 8M (0.50%)

Stiff ODE  
system

$$\frac{dY_j}{dt} = S_j$$

Jacobian  
matrix

$$J_{ij} = \frac{dS_i}{dY_j}$$



Implicit  
methods

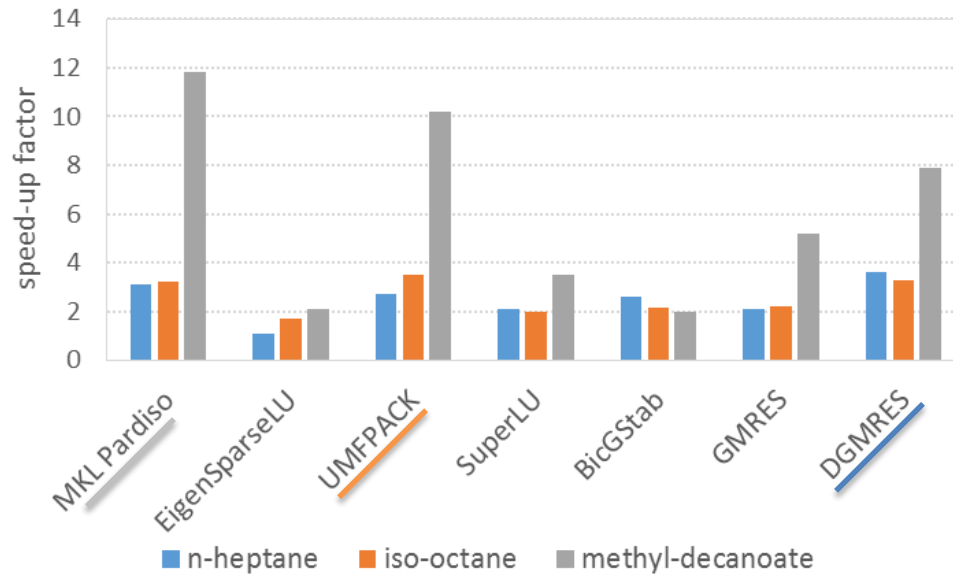
OpenSMOKE++ ODE solver was extended  
to sparse systems

- EigenSparseLU
- MKL Pardiso
- UMFPACK
- SuperLU (serial)

Direct  
solvers

- BiCGStab
- GMRES
- DGMRES

Iteratives  
solvers

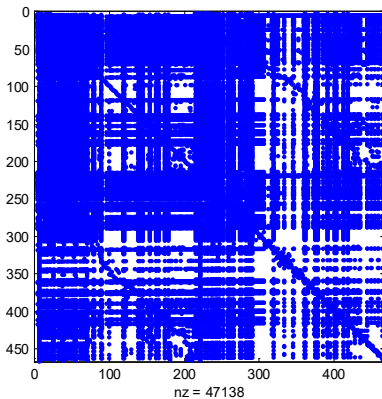
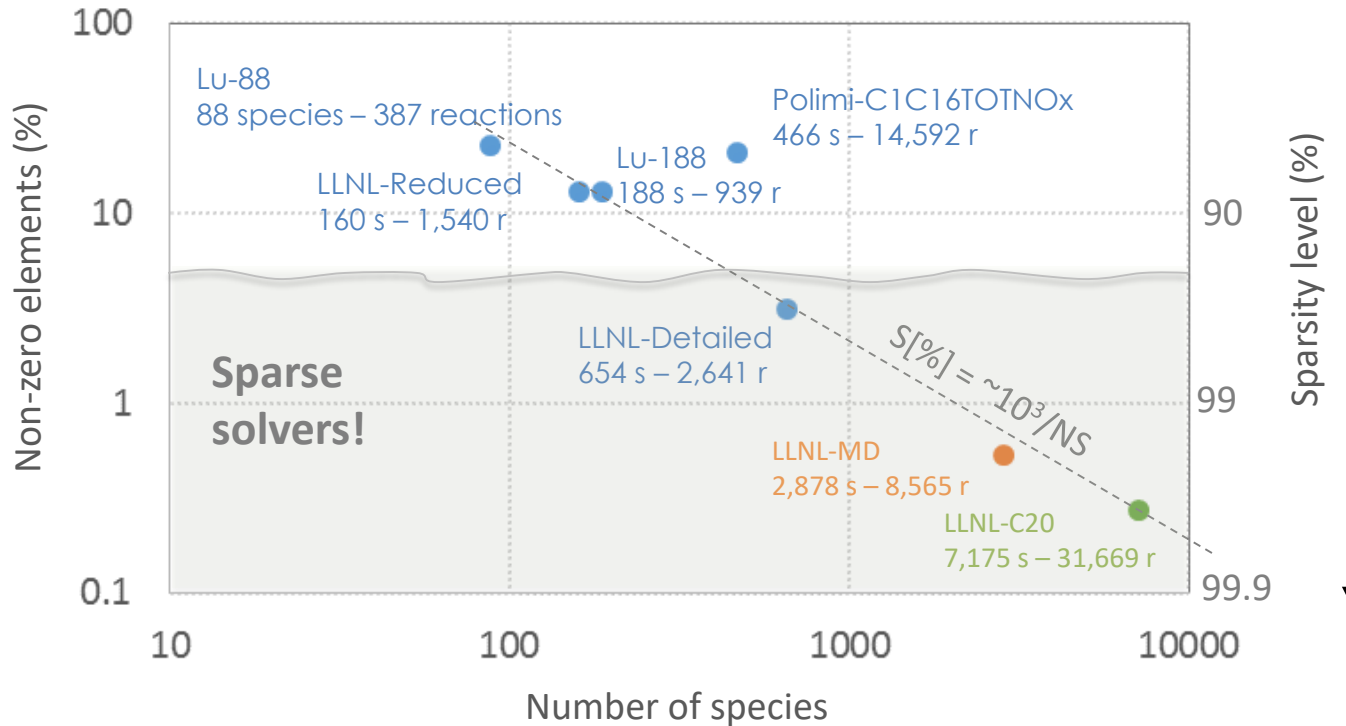


Speed-up factors of sparse linear solvers with respect to the OpenSMOKE++ dense solver

	n-heptane	Iso-octane	Methyl-decanoate
Species	658	878	2878
Reactions	2827	3769	8555
Non-zero elements	13151	18,471	44,620
% sparsity	97%	97.7%	99.5%

The larger the sparsity of a kinetic mechanism, the larger the speed-up factor in using a sparse linear solver

# Sparse linear solvers for detailed chemistry (II)



Polimi-C1C16TOTNOx  
466 species  
14,592 reactions  
Sparsity = 79%



- The sparsity level of a mechanism is also a function of the technique adopted for its development
- Adoption of sparse algorithms is convenient only if the sparsity is sufficiently high (**>95%**)

The cost for a chemical step in a CFD simulation carried out on a grid with  $N$  cells is:

$$C_{chem} \sim N \times N_S^\alpha \quad \text{with } \alpha = 2 \div 3$$

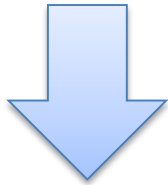
Under the assumption that  $N \gg N_S$ , it is possible to demonstrate that the cost of PCA scales as:

$$C_{PCA} \sim N \times N_S^2$$

Thus, **the relative cost of PCA with respect to the chemical step does not increase with the size of the mesh** and it is expected to slightly decrease with the number of species:

$$\frac{C_{PCA}}{C_{chem}} \sim \frac{1}{N_S^{\alpha-2}}$$

On which basis can reacting cells be regarded as similar or different?



## Clustering algorithms

The grouping of computational cells, in the calculation domain, into clusters is achieved by using **clustering algorithms** which identify cells that have similar thermochemical states.

How to conservatively redistribute the species among the cells, after integration?

**Liang L., Stevens J. G., Farrell J.T.**, *A Dynamic Multi-Zone Partitioning Scheme for Solving Detailed Chemical Kinetics in Reactive Flow Computations*, Combustion Science and Technology 181(11), p.1345-1371 (2009)

**G.M. Goldin, Z. Ren, S. Zahirovic**, *A cell agglomeration algorithm for accelerating detailed chemistry in CDF*, Combust. Theory Model., 13, pp. 721–739 (2009)



A simple, weighted remapping of the species mass fractions changes from the cluster is not able to ensure mass conservation and it would gradually deteriorate the solution.

Mass fraction change in cluster  $k$   
(over time step  $\Delta t = t^{n+1} - t^n$ )

$$\Delta Y_{k,j} = Y_{k,j}^{n+1} - Y_{k,j}^n$$

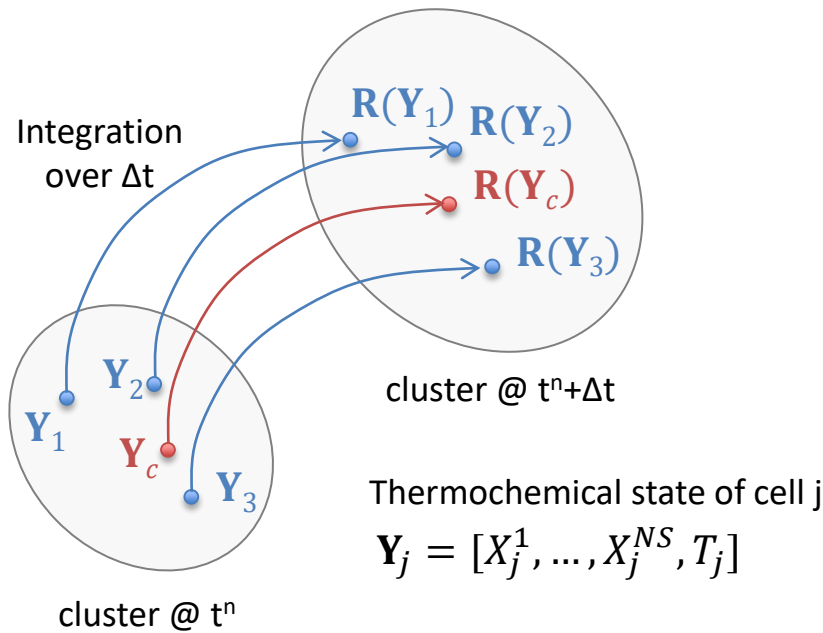


Change of species partial density  
to be mapped back to the original cells  $i$

$$\rho_{i,j}^{n+1} = \rho_{i,j}^n + \begin{cases} \Delta Y_{k,j} \rho_i^n & \text{if } \Delta Y_{k,j} \geq 0 \\ \Delta Y_{k,j} \rho_k^n \frac{\rho_{i,j}^n}{\rho_{k,j}^n} & \text{if } \Delta Y_{k,j} < 0 \end{cases}$$

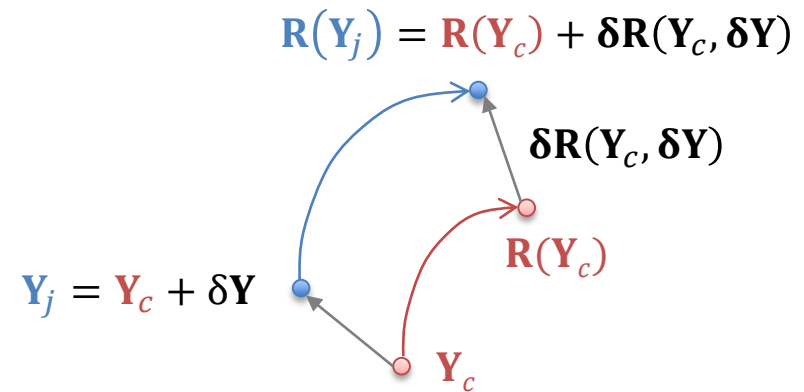
The cells' temperatures are estimated from the updated mixture sensible enthalpy.

Liang L., Stevens J. G., Farrell J.T., *A Dynamic Multi-Zone Partitioning Scheme for Solving Detailed Chemical Kinetics in Reactive Flow Computations*, Combustion Science and Technology 181(11), p.1345-1371 (2009)



Chemical step: ODE integration

$$\mathbf{R}(\mathbf{Y}_j) = \int_{t^n}^{t^n + \Delta t} \mathbf{f}(\mathbf{Y}_j, \mathbf{Y}, t) dt$$

$$\mathbf{R}(\mathbf{Y}_j) = \mathbf{R}(\mathbf{Y}_c) + \delta \mathbf{R}(\mathbf{Y}_c, \delta \mathbf{Y})$$


$$\mathbf{Y}_j = \mathbf{Y}_c + \delta \mathbf{Y}$$

$$\delta \mathbf{R}(\mathbf{Y}_c, \delta \mathbf{Y})$$

$$\mathbf{R}(\mathbf{Y}_c)$$

$$\mathbf{Y}_c$$

If  $\delta \mathbf{Y}$  is small enough:

$$\mathbf{R}(\mathbf{Y}_j) \approx \mathbf{R}(\mathbf{Y}_c) + \left. \frac{\partial R^i}{\partial Y^k} \right|_{\mathbf{Y}_c} \delta \mathbf{Y} = \mathbf{R}(\mathbf{Y}_c) + \mathbf{S} \cdot \delta \mathbf{Y}$$

Matrix of linearized mapping gradients

$$S_{ik} = \left. \frac{\partial R_i}{\partial Y^k} \right|_{\mathbf{Y}_c}$$

Pope S.B., "Combustion Theory and Modelling, 1 (1997) 41-63

$$\mathbf{R}(\mathbf{Y}_j) \approx \mathbf{R}(\mathbf{Y}_c) + \left. \frac{\partial R^i}{\partial Y^k} \right|_{\mathbf{Y}_c} \delta \mathbf{Y} = \mathbf{R}(\mathbf{Y}_c) + \mathbf{S} \cdot \delta \mathbf{Y}$$

F. Perini, R.D. Reitz, Frontiers in Computational Physics: Energy Sciences Zurich, Switzerland June 5, 2015

The linear mapping gradients are the **first-order sensitivities** of the ODE system w.r.t. the initial conditions evaluated at the final integration time:

$$\begin{cases} \frac{d\mathbf{S}}{dt} = \mathbf{J}(t, \mathbf{Y}) \cdot \mathbf{S}(t, \mathbf{Y}) \\ \mathbf{S}(t, \mathbf{Y}_c) = \mathbf{I} \end{cases}$$

- Dense, stiff ODE system with  $N_S^2$  equations
- Computationally too expensive to be solved on-the-fly



**Linearized solution mapping in the PC space (i.e., reduced sensitivity system):**

$$\mathbf{R}(\mathbf{p}_j) \approx \mathbf{R}(\mathbf{p}_c) + \left. \frac{\partial R^i}{\partial p^k} \right|_{\mathbf{p}_c} \delta \mathbf{p} = \mathbf{R}(\mathbf{p}_c) + \tilde{\mathbf{S}} \cdot \delta \mathbf{p}$$

Matrix of linearized mapping gradients  $\tilde{s}_{ik} = \left. \frac{\partial R_i}{\partial p^k} \right|_{\mathbf{p}_c}$  only  $N_{PC}^2$  elements

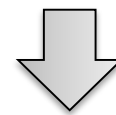
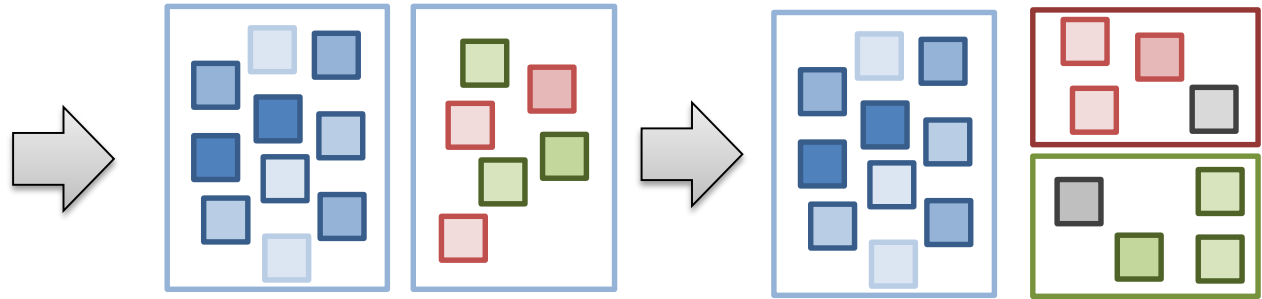
# Dynamic Multi-Zone (DMZ) clustering

As opposed to static algorithms such as a basic k-means algorithm, the DMZ algorithm (Liang 2009) does not require the *a priori* specification of the number of zones.

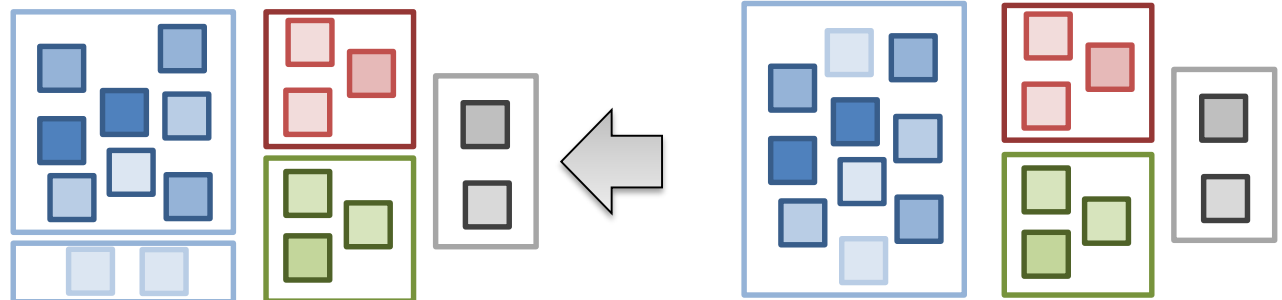
the algorithm starts by initializing all the cells as 1 big zone

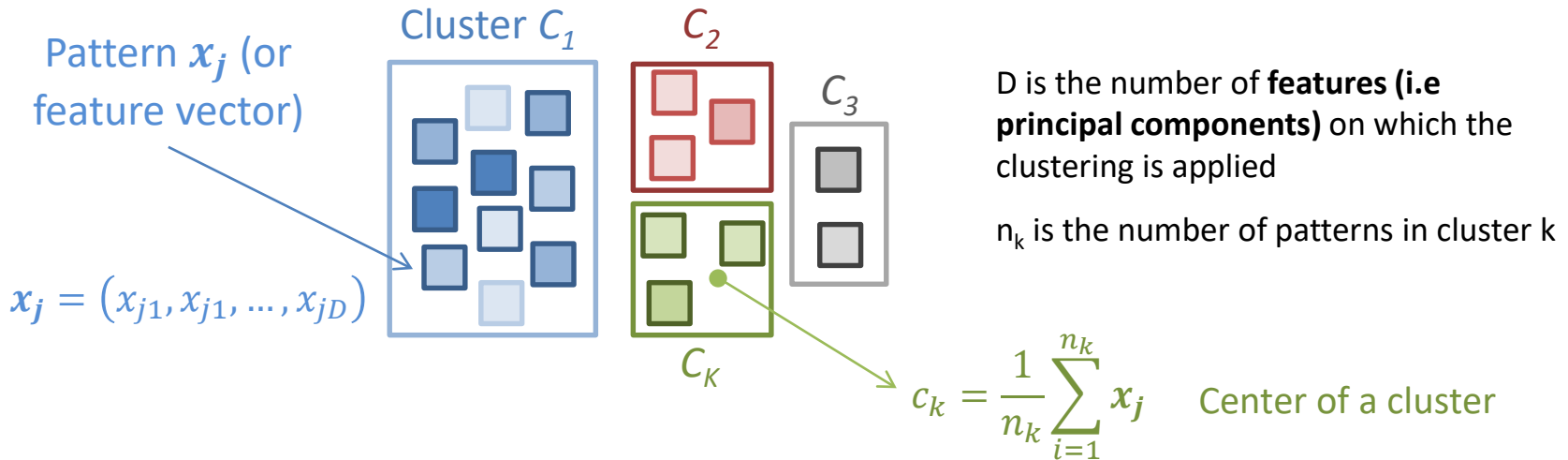


the number of zones evolves as bigger zones are split into smaller ones via a **bisection-splitting** algorithm



the algorithm terminates when the dispersion metrics become smaller than **user-specified tolerance  $\epsilon$**  in all zones.





Distance between the  $d^{th}$  feature

$$dist^{(d)}(x_i^{(d)}, x_i^{(d)}) = |x_i^{(d)} - x_i^{(d)}|$$

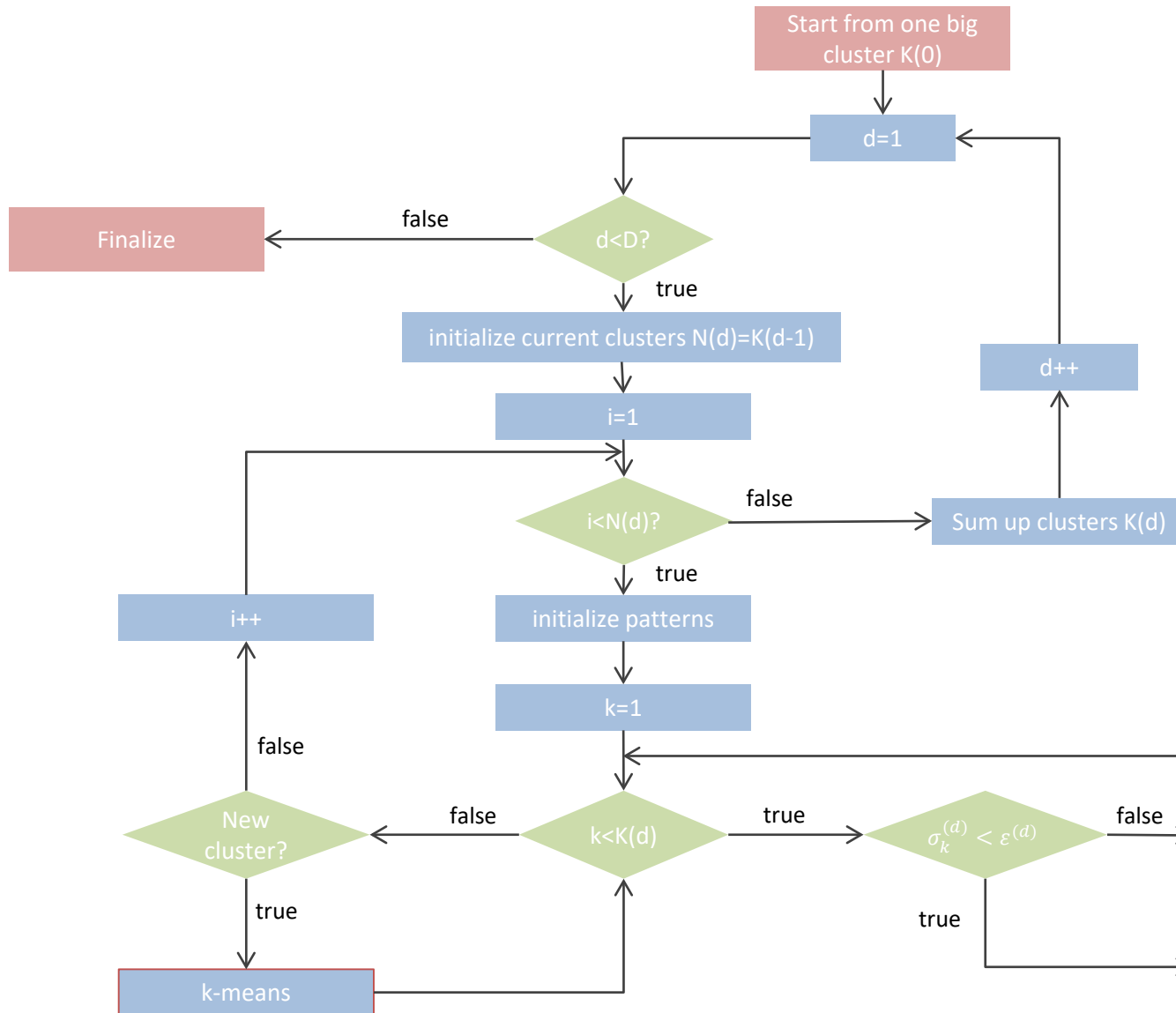
Dispersion of feature  $d$  in cluster  $C_K$

$$\sigma_k^{(d)} = \max \{ dist^{(d)}(x_i^{(d)}, x_i^{(d)}) \}$$

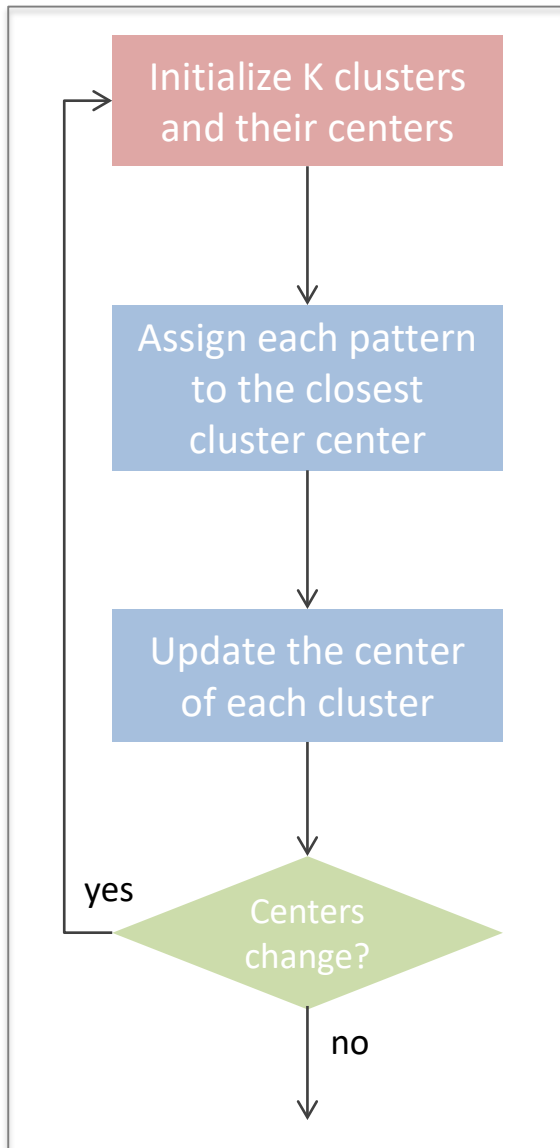
Clustering in each dimension  $d$  is terminated when the dispersion becomes smaller than the user-specified tolerance  $\epsilon^{(d)}$  in all clusters and **in all dimensions**:

$$\sigma_k^{(d)} < \epsilon^{(d)}$$

# Dynamic Multi-Zone (DMZ) partitioning (II)

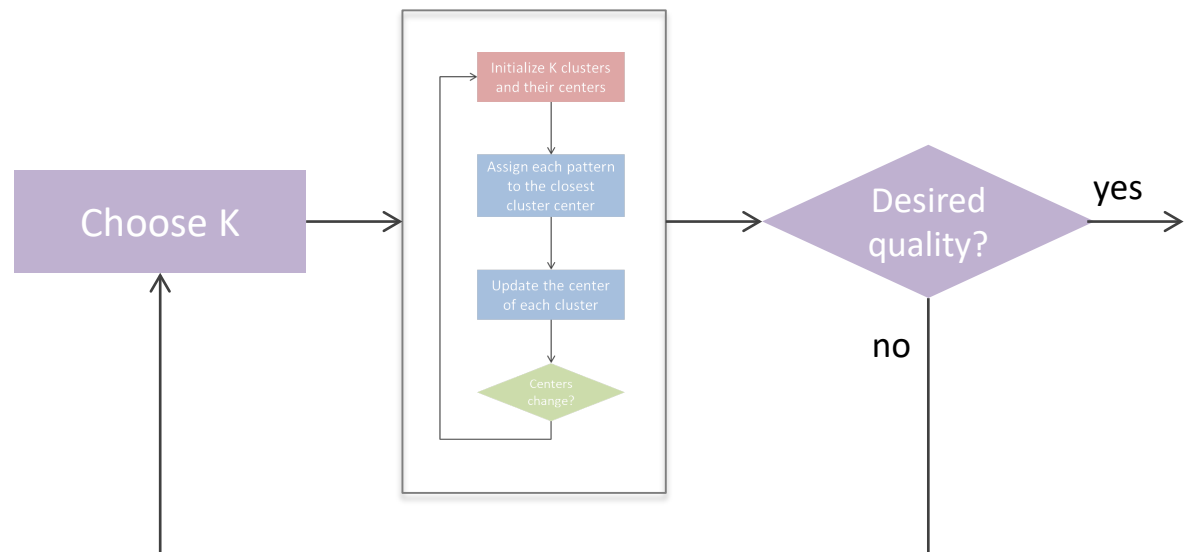


at stage  $d$ , each of the  $K(d-1)$  clusters generated from stage  $d-1$  is treated as a new clustering task, and each task independently breaks down a stage  $d-1$  cluster into smaller ones until all newly generated clusters satisfy the termination criterion defined by the  $d$  feature



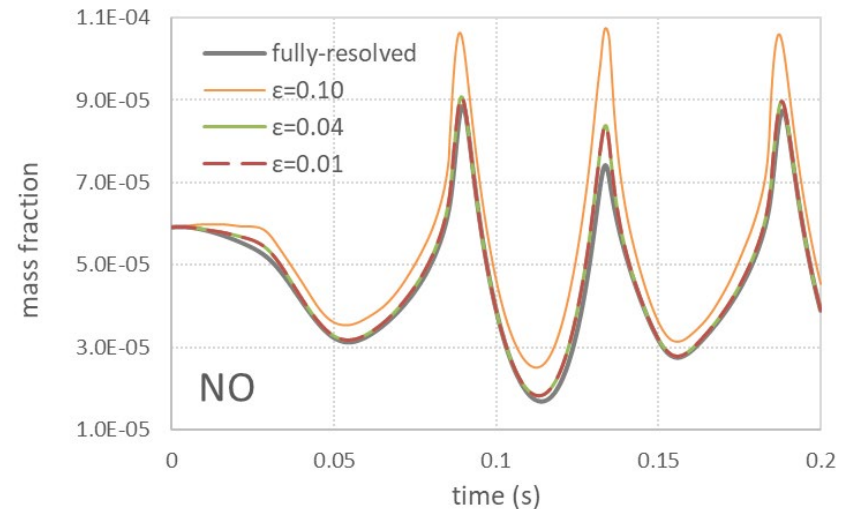
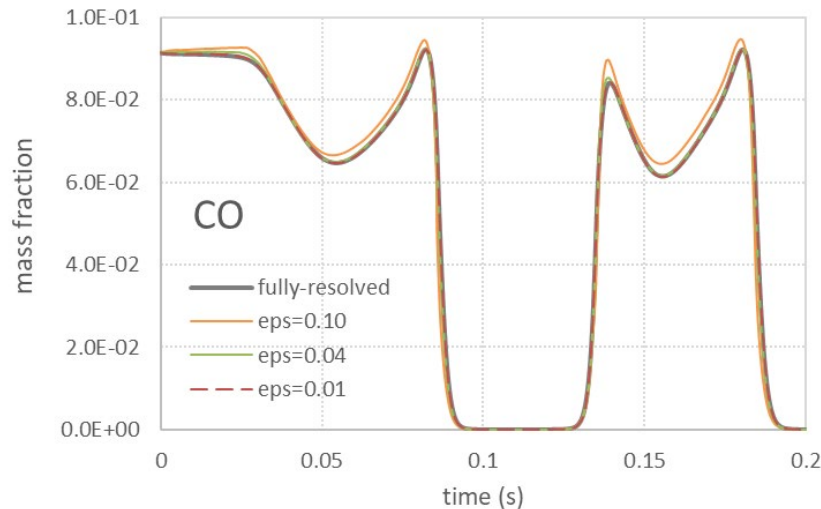
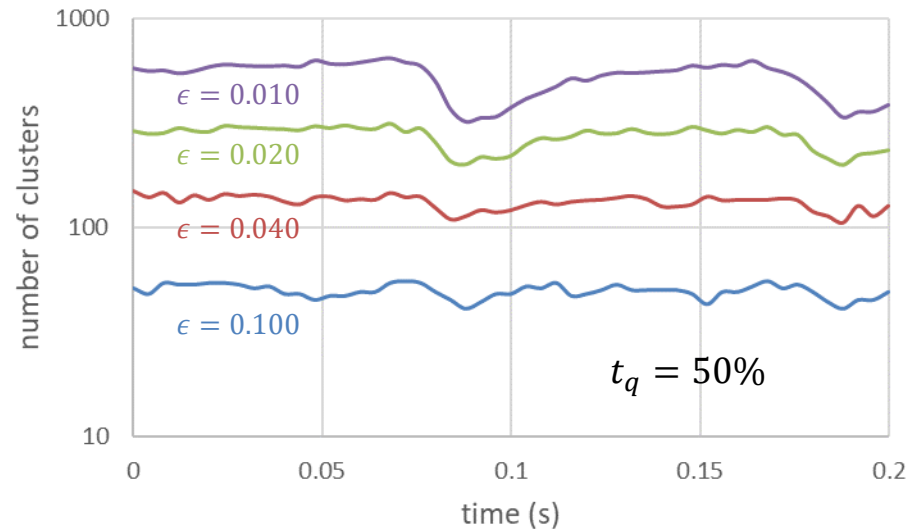
One of the major problems of data clustering via k-means is represented by the estimation of the optimal number of clusters  $K$

Typically, the k-means clustering algorithm is repeated at increasing number of partition clusters  $K$ , and that is stopped after that the desired partition quality has been reached. This process of course is very computationally expensive

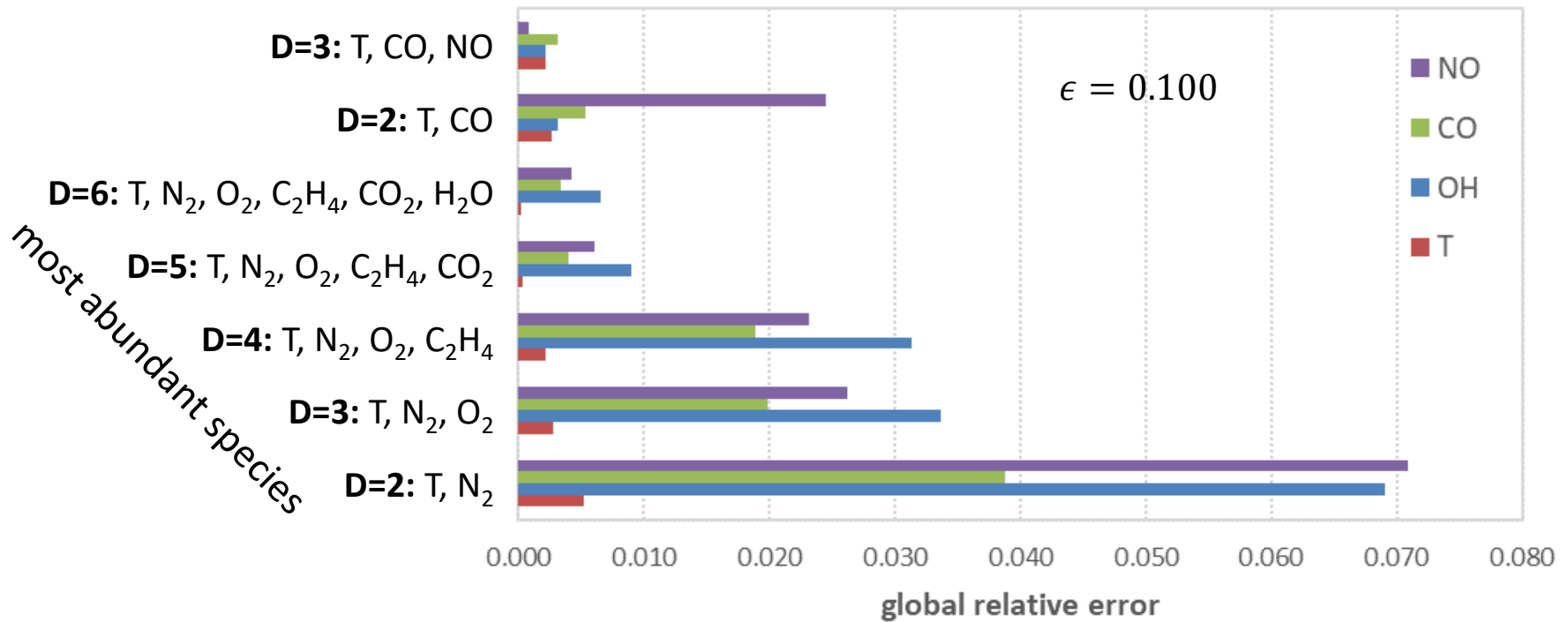


# Impact of user-defined tolerance $\epsilon$

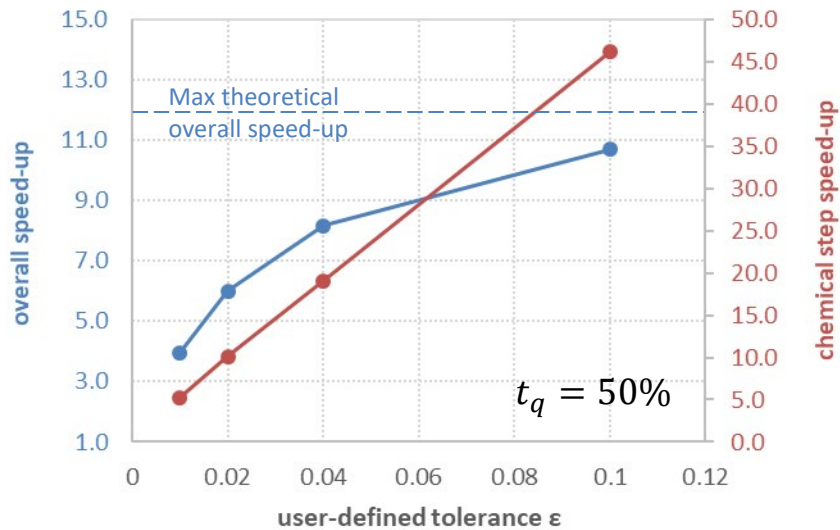
Number of clusters as a function of the user-defined clustering tolerance  $\epsilon$



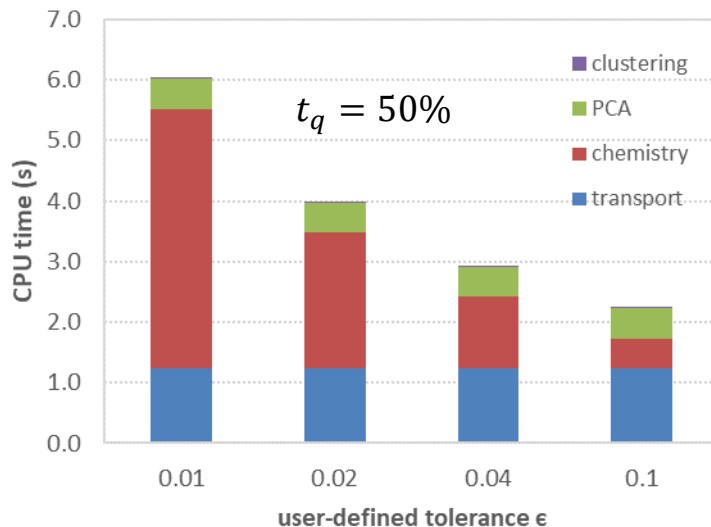




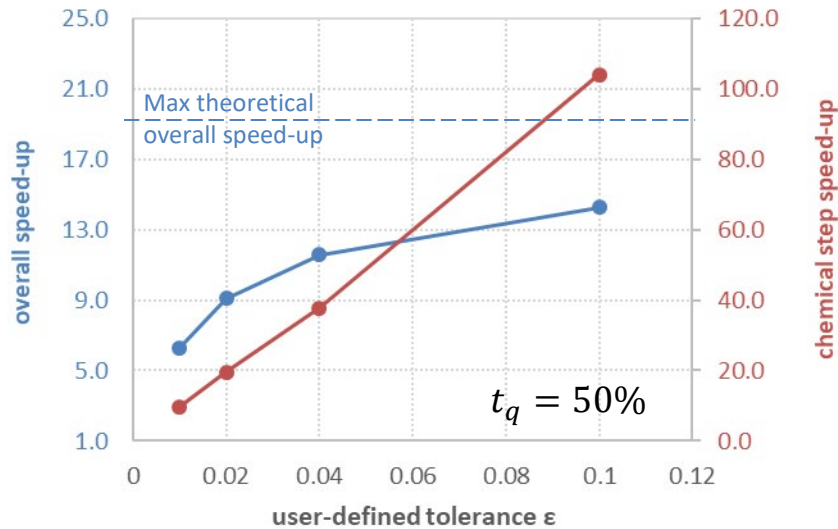
- the results are very sensitive to the choice of the  $D - 1$  species
- the overall error is systematically larger than the corresponding  $P(CA)^2$  simulation carried out with the same values of  $D$  and  $\epsilon$



- As expected, the overall computational cost of the CA-based simulation decreases monotonically with increasing tolerances.
- The saving in CPU time impacts the chemical step only



- The PCA computational time does not depend on the clustering parameters  $t_q$  and  $\epsilon$
- The clustering time is negligible

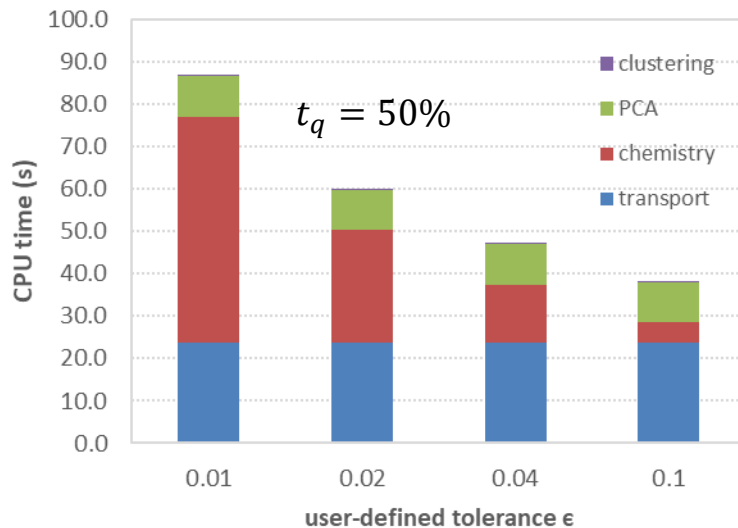


## Kinetic mechanism

224 species and 5939 reactions

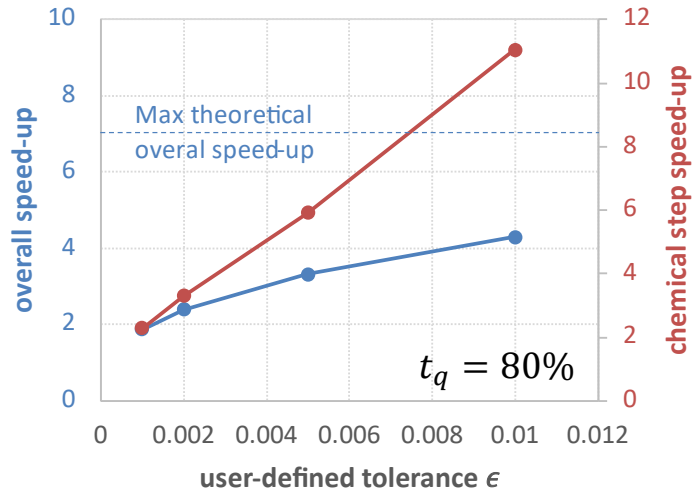
PAH chemistry included  
(up 2 aromatic rings)

- By increasing  $t_q$  and/or decreasing the tolerance  $\epsilon$ , the accuracy of the CA-based simulation increases monotonically
- Also in this case, the cost associated with the clustering algorithm is negligible, despite the higher number of species.
- As expected, the cost of the PCA step ( $\sim 10$  s) increases in terms of absolute values, but it is still only  $\sim 2\%$  of the computational time of the original chemical step ( $\sim 520$  s).



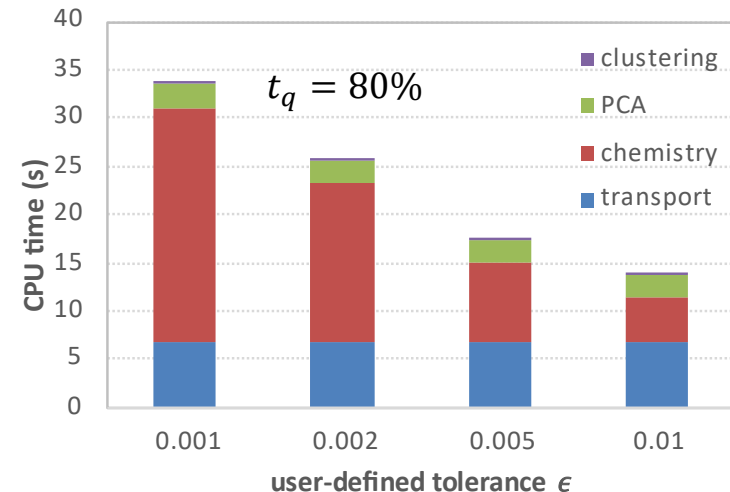
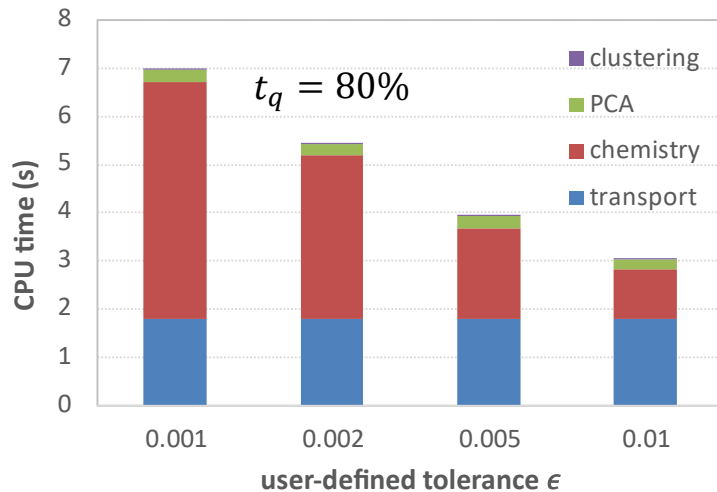
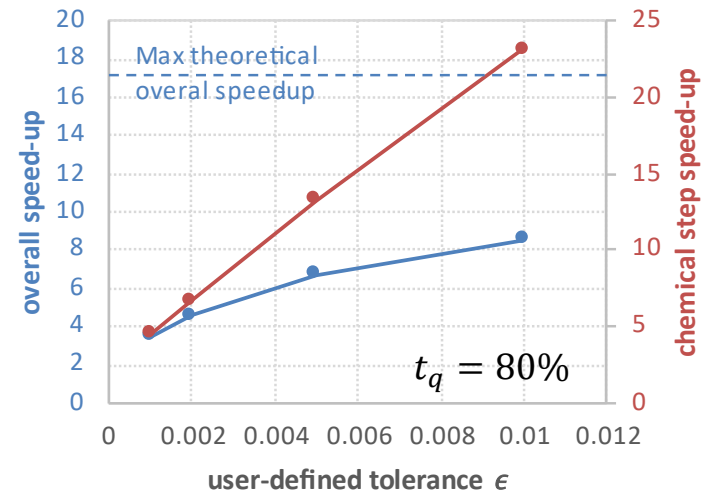
## Hawkes (2007) mechanism (11 species)

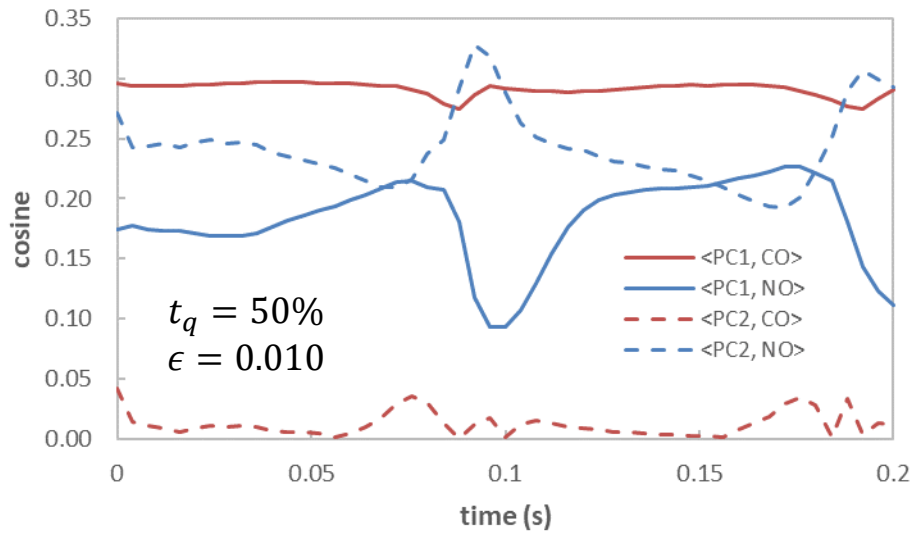
Chemistry CPU time: 86%



## CRECK2003NOX mechanism (57 species)

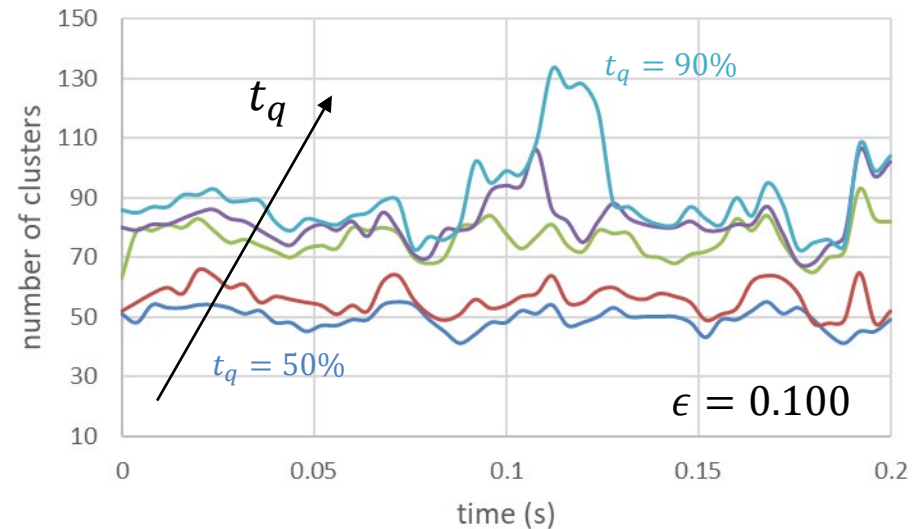
Chemistry CPU time: 95%

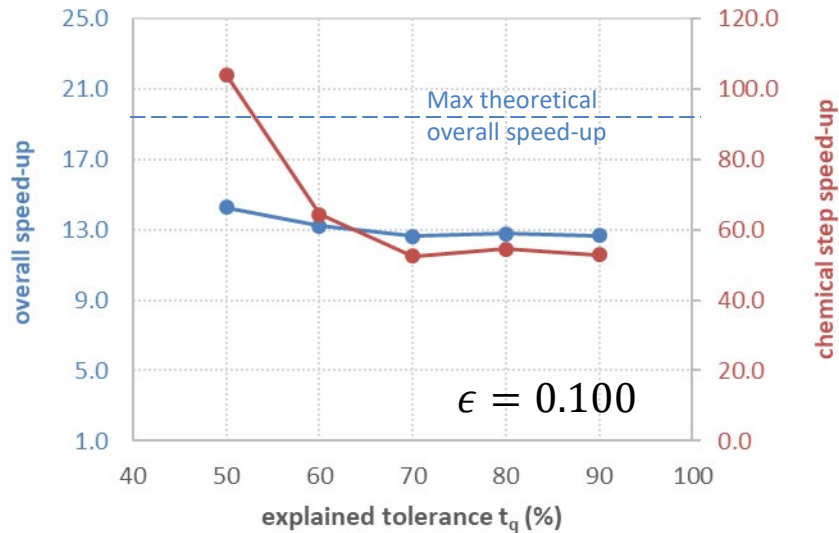




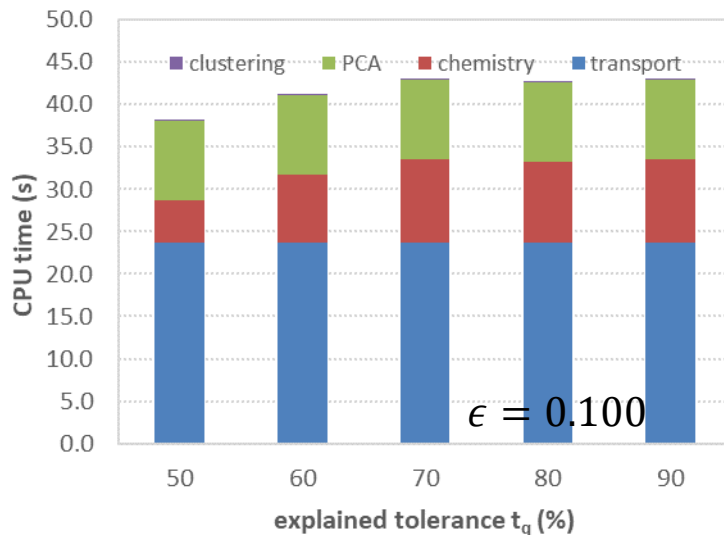
Temporal evolution of cosine values of the angles between the first 2 principal axes and species CO and NO

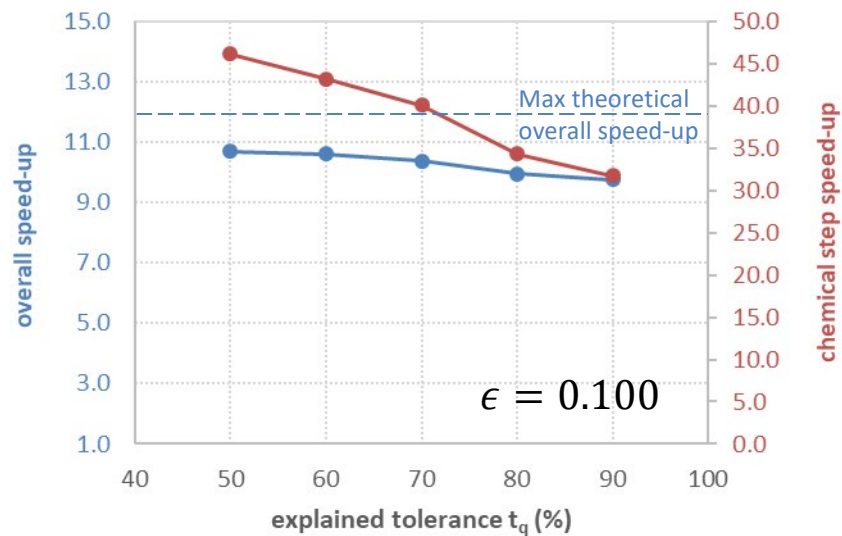
Number of clusters as a function of the user-defined explained variance  $t_q$



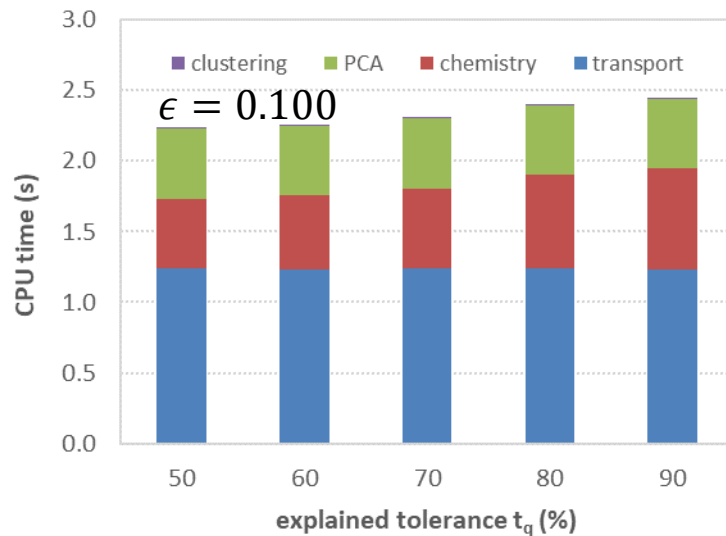


- By increasing the number of features  $D$  and/or decreasing the tolerance  $\epsilon$ , the accuracy of the CA-based simulation increases monotonically
- Also in this case, the cost associated with the clustering algorithm is negligible, despite the higher number of species.
- As expected, the cost of the PCA step ( $\sim 10$  s) increases in terms of absolute values, but it is still only  $\sim 2\%$  of the computational time of the original chemical step ( $\sim 520$  s).





- As expected, the overall computational cost of the CA-based simulation decreases monotonically with increasing tolerances.
- The saving in CPU time impacts the chemical step only



- The PCA computational time does not depend on the clustering parameters  $t_q$  and  $\epsilon$
- The clustering time weakly increases with the increasing number of features, but it is basically negligible

## ISF F3 flames

Internal diameter: 4 mm

Velocities: 35 cm/s

Fuel composition: 80% C<sub>2</sub>H<sub>4</sub> + 20% N<sub>2</sub>

## Artificially imposed sinusoidal fluctuations of fuel stream velocity

Amplitude: 90%

Frequency: 10 Hz

## Kinetic mechanism

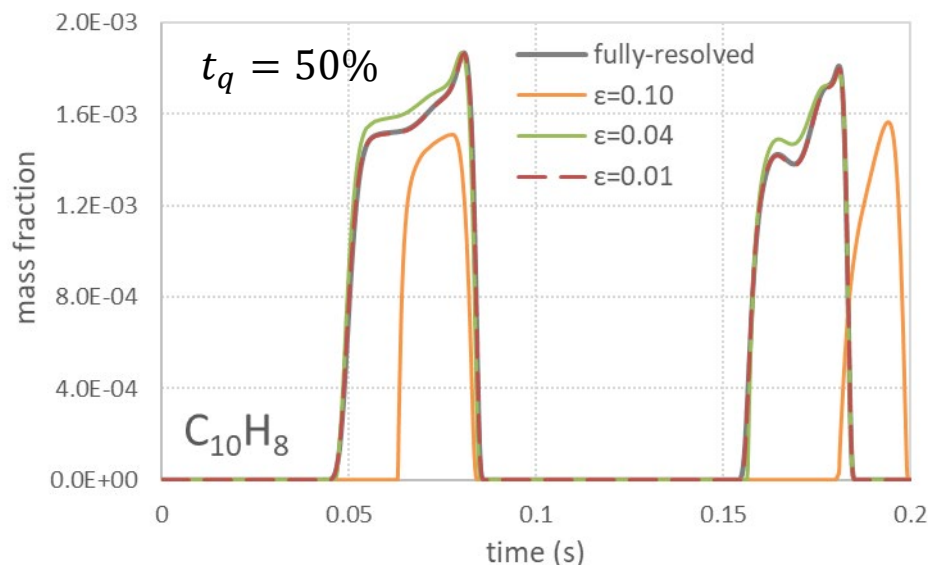
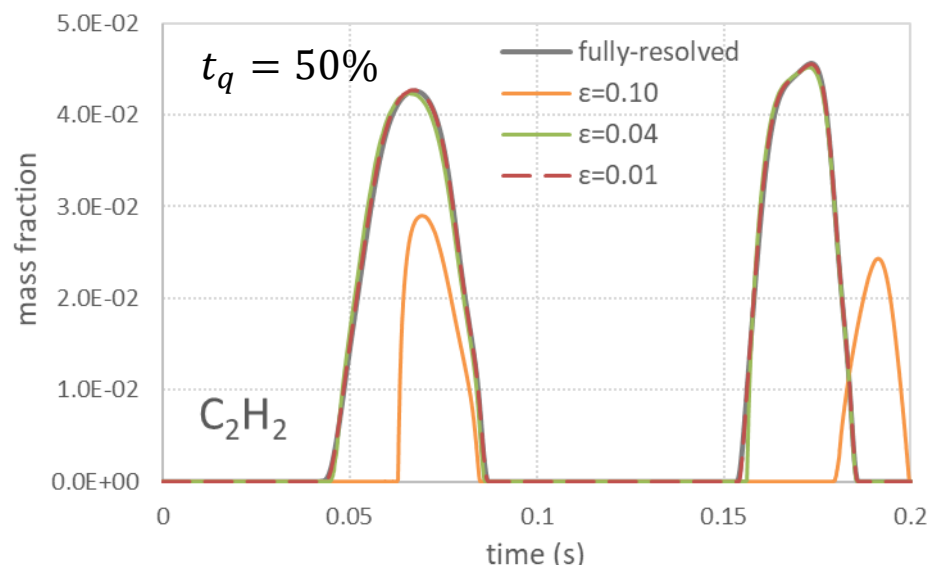
224 species and 5939 reactions

PAH chemistry included  
(up 2 aromatic rings)

## Computational domain

2D region (55 x 120 mm)

~25,000 cells



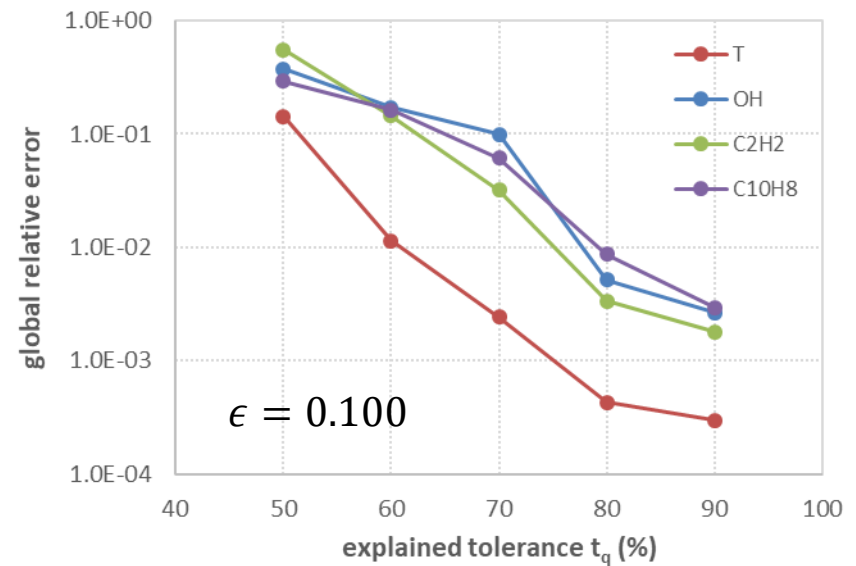
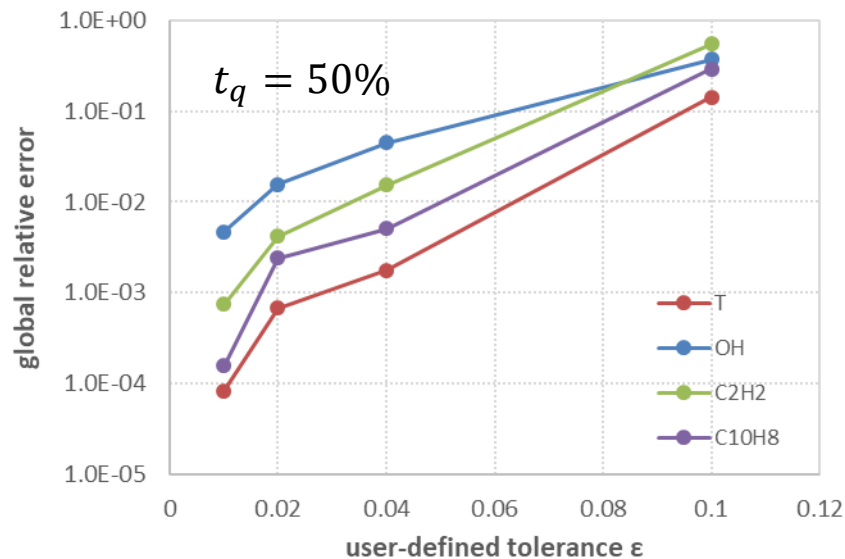


Global relative error

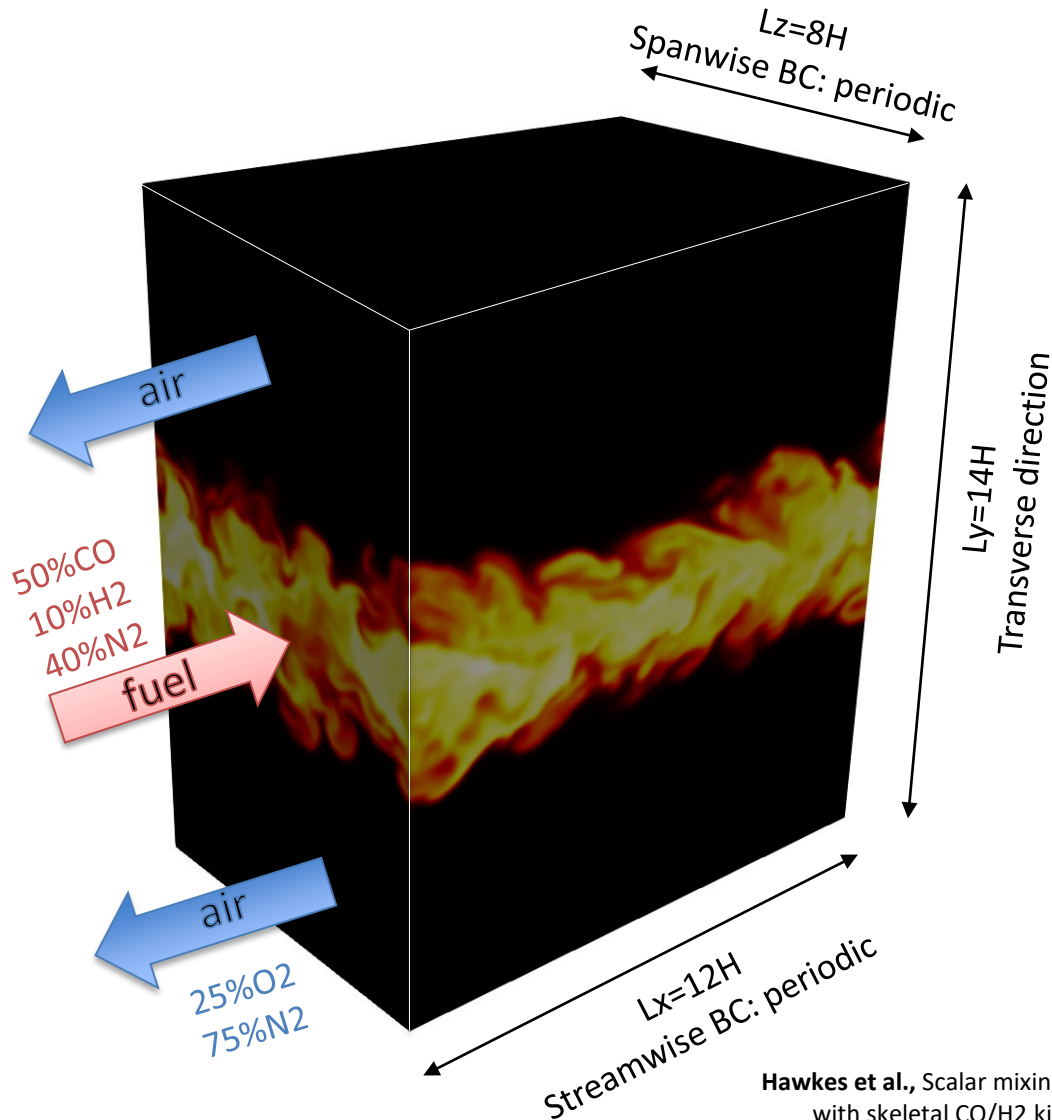
$$\varepsilon = \frac{1}{N_C N_T} \sum_{k=1}^{N_T} \sum_{i=1}^{N_C} \frac{|\psi_{k,i}^{CA} - \psi_{k,i}|}{\psi_{max}}$$

$\psi_{k,i}$  fully-resolved solution in cell  $i$  at time  $k$

$\psi_{k,i}^{CA}$  CA-based solution in cell  $i$  at time  $k$



# Temporally-evolving planar jet-flame



## Flame H

$H = 1.37 \text{ mm}$

$Re = 9079$

$t_j = 4.96 \mu\text{s}$

$U = 276.4 \text{ m/s}$

$Da = 0.011$

$Ma = 0.30$

## Quasi-DNS

$\Delta x = 45 \mu\text{m}$

Mesh:  $365 \times 426 \times 243$

Cells:  $\sim 37.8\text{M}$

## Solver

laminarSMOKE++ (based on OF-9)

<https://github.com/acuoci/laminarSMOKE>

Time discretization: implicit 2nd order

backward Euler

Space discretization: OF *cubic* scheme

Hawkes et al., Scalar mixing in direct numerical simulations of temporally evolving plane jet flames with skeletal CO/H<sub>2</sub> kinetics, Proceedings of the Combustion Institute, 31, p. 1633-1640 (2007)

**Sensitivity analysis** to PCA<sup>2</sup> parameters were carried out on 2D cases

- explained variance
- clustering tolerances

## 2D Mesh

$\Delta x = 30 \mu\text{m}$  or  $45 \mu\text{m}$

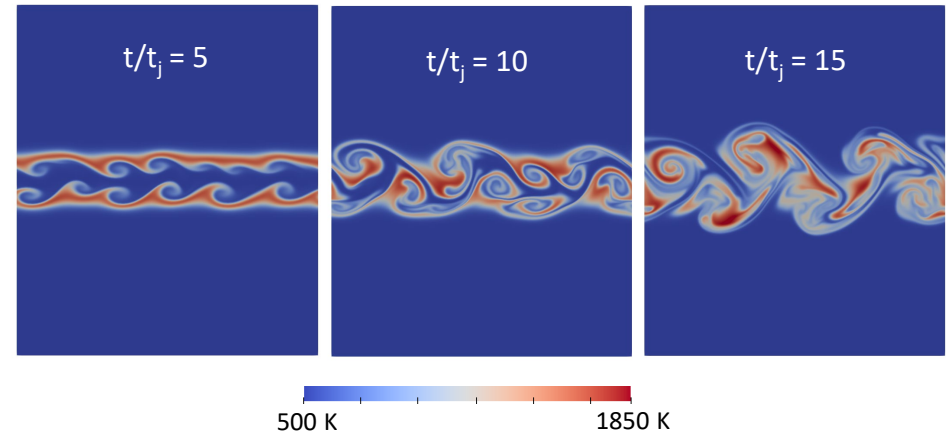
Mesh: 548x640 or 365x426

Cells: ~350k or ~156k

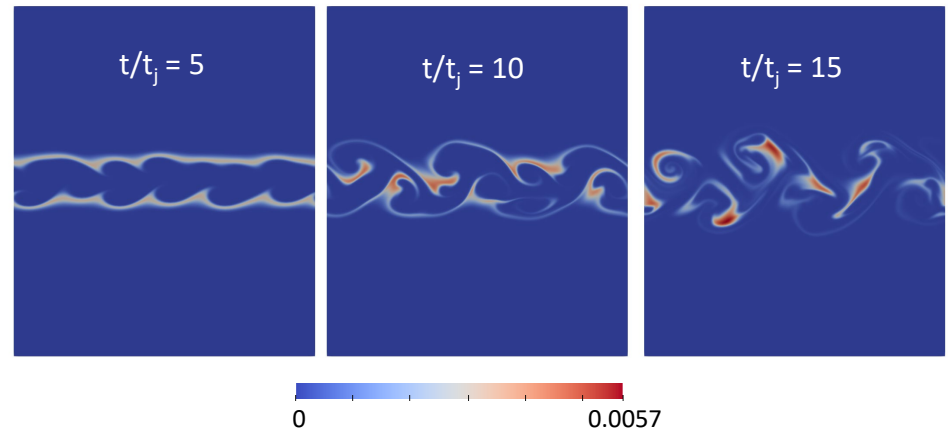
## Kinetic mechanisms

- Skeletal H<sub>2</sub>/CO mechanism by **Hawkes** et al. (2007): 11 species and 21 reactions
- Detailed H<sub>2</sub>/CO + NO<sub>x</sub> mechanism by **CRECK** Modeling Lab: 57 species and 385 reactions

Temperature

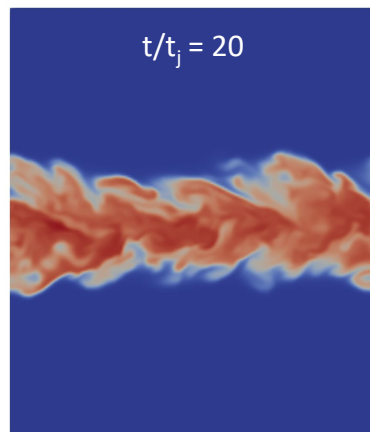
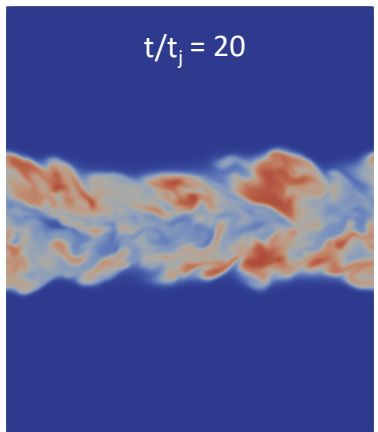
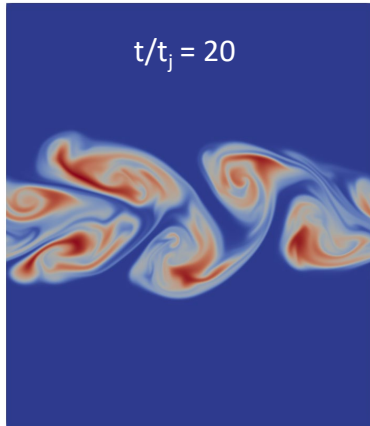


OH mass fraction



temperature

mixture fraction



Stanley et al. (1998)

2D and 3D flows are **qualitatively very different**

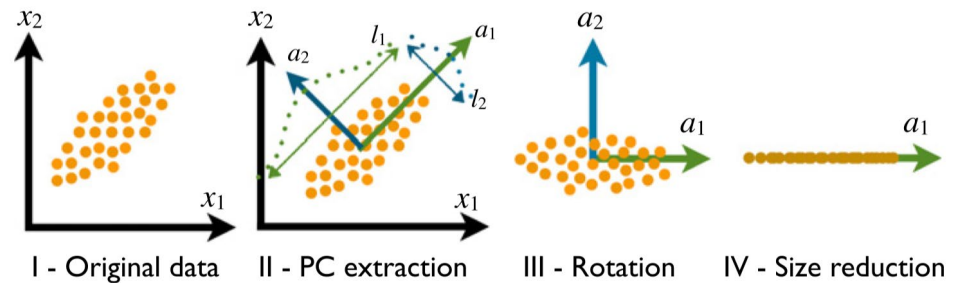
- 2D jets are dominated by a large vortex dipole instability, which does not occur in 3D
- in 2D, large coherent structures
- in 2D, over-prediction of extinguished states
- in 3D, more small-scale structures
- In 3D, high-dissipation structures are more transient

$$\mathbf{X} = \begin{matrix} \text{Instantaneous snapshot} \\ \begin{bmatrix} x_{11} & x_{12} & \dots & x_{1Q} \\ x_{21} & x_{22} & \dots & x_{2Q} \\ \vdots & \vdots & \ddots & \vdots \\ x_{n1} & x_{n2} & \dots & x_{nQ} \end{bmatrix} \end{matrix} \begin{matrix} \text{State variable} \\ \end{matrix} = \begin{bmatrix} T^1 & Y_1^1 & \dots & Y_p^1 \\ T^2 & Y_1^2 & \dots & Y_p^2 \\ \vdots & \vdots & \ddots & \vdots \\ T^n & Y_1^n & \dots & Y_p^n \end{bmatrix}$$

Rows represent observations and columns correspond to the problem variables (T, and species mass fraction).

Covariance matrix

$$\mathbf{S} = \mathbf{X}^T \mathbf{X} \longrightarrow \mathbf{S} = \mathbf{A} \mathbf{L} \mathbf{A}^T$$



**PC (Principal Components):** eigenvectors of S, i.e. the columns of A

**Eigenvalues:** i.e. the diagonal of the L matrix, the portion of variance they account for.



## Problem

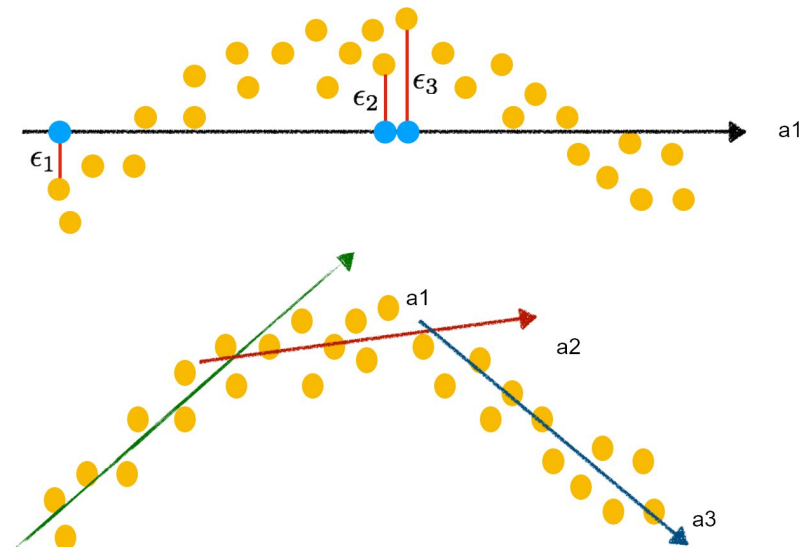
Because PCA is a linear combination of basis function, for **highly non-linear systems** such as combustion applications, a large number of PCs is required to describe the problem properly.

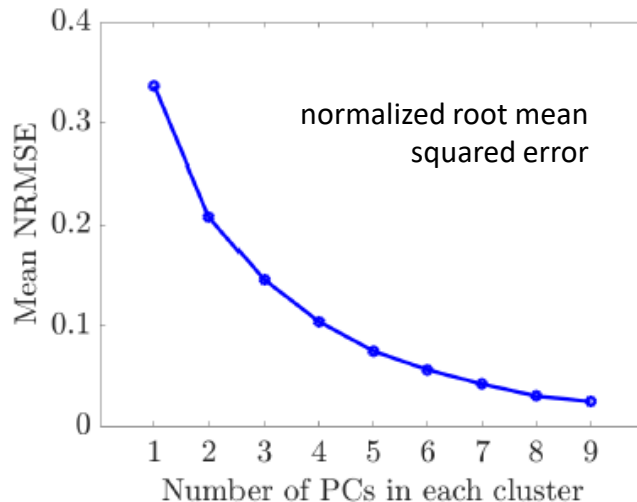
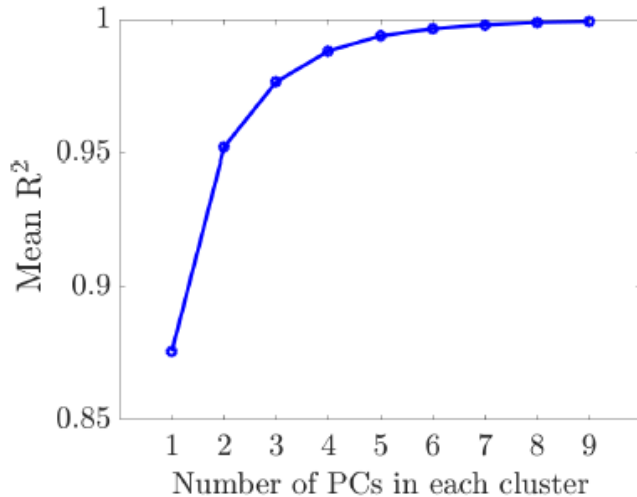


## Solution

With a **local formulation of PCA (LPCA)** we overcome this problem.

The LPCA finds clusters of data which are characterized by similar properties. In each cluster PCA is performed, and a set of local PCs is found





## 1. Initialization

The initial clusters centroids are chosen from a **k-means solution**. The eigenvector matrix in each cluster is initialized as the identity matrix.

## 2. Partition

Each observation is assigned to a cluster by means of the calculation of a reconstruction error.

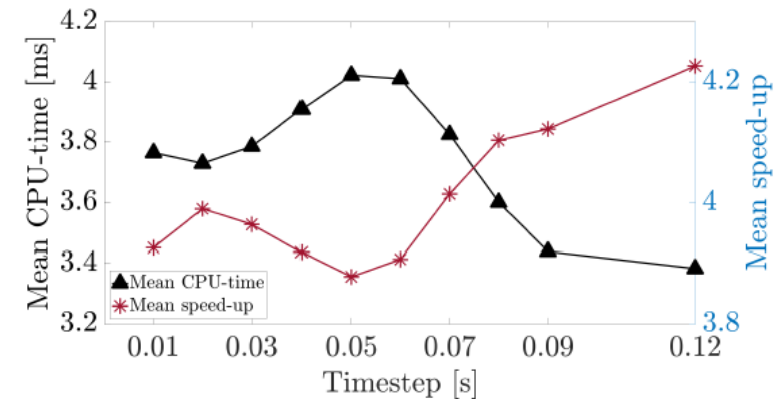
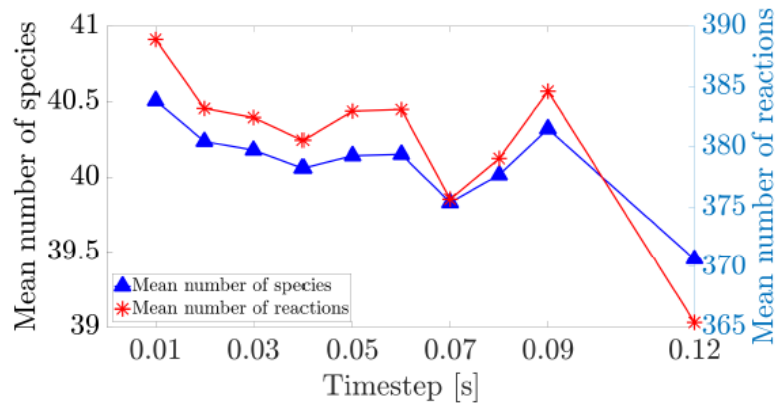
## 3. Update

The cluster centroids are updated on the basis of the partitioning carried out at step 2.

## 4. Local-PCA

LPCA is performed in each cluster found at step 2.

# Unsteady flame: new conditions (II)



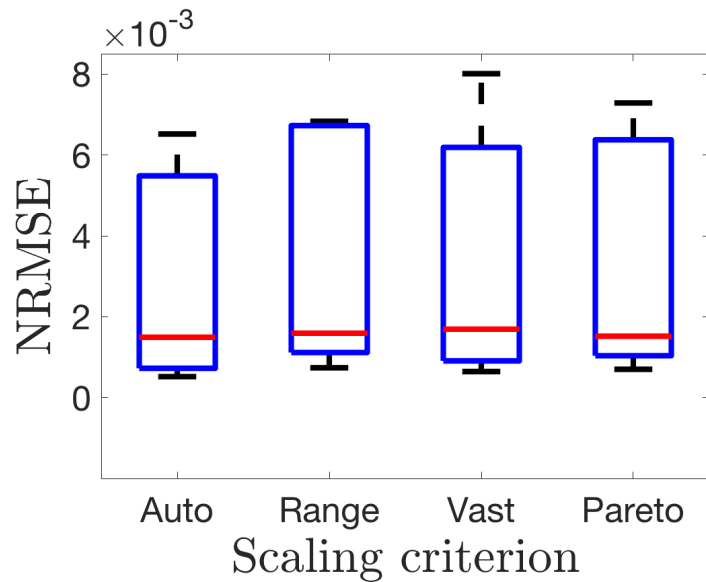
The average number of active species and reactions change in time because of the flame evolution

The active species and active reactions are strictly correlated

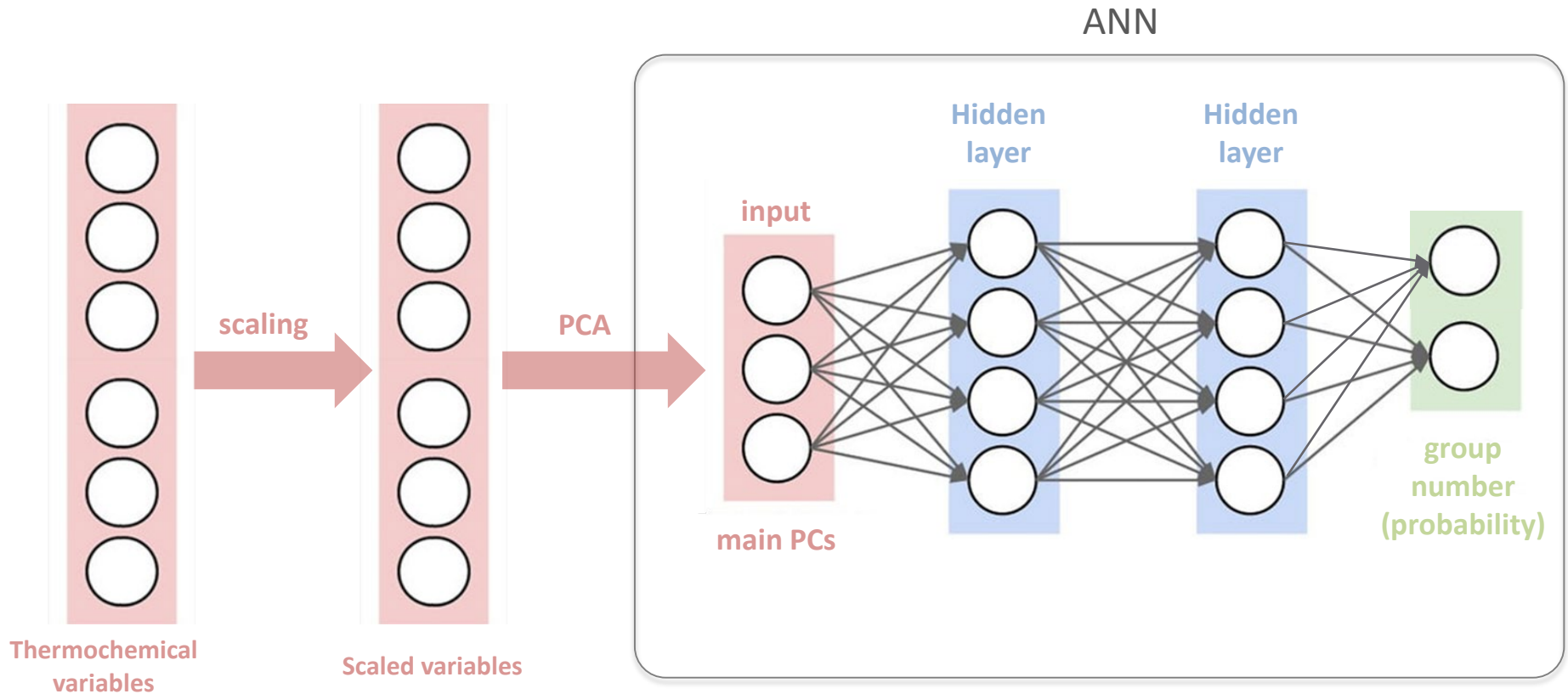
The CPU time is strongly dependent on the number of species



The scaling criterion has a reduced effect on the chemical reduction and consequently on the adaptive simulation accuracy



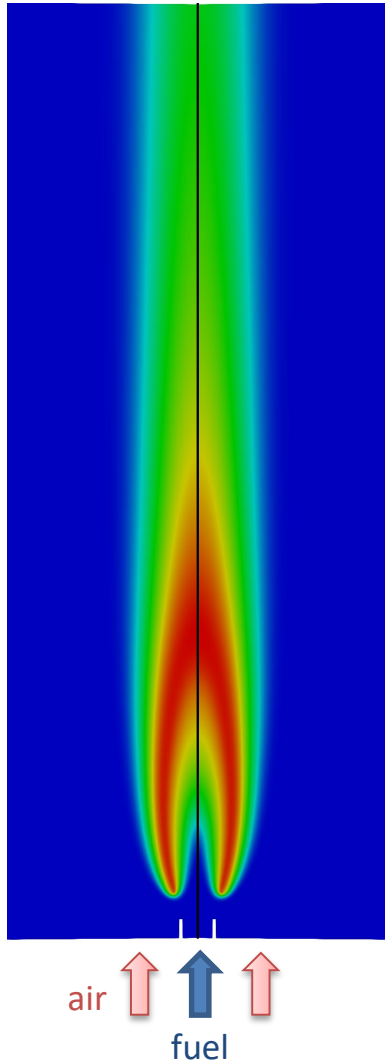
$\varepsilon_{DRGEP}$	$n_{sp}^{mean}$	$n_{sp}^{max}$	$\lambda_{mean}$
AUTO	43	50	0.071
PARETO	41	51	0.070
VAST	43	52	0.074
RANGE	40	48	0.074



The ANN solves a **multi-class classification** problem

D'Alessio G., Cuoci A., Parente A., *Feature extraction and artificial neural networks for the on-the-fly classification of high-dimensional thermochemical spaces in adaptive-chemistry simulations*, Data-Centric Engineering (2020)

# A test case: steady-state laminar coflow flame



## Fuel stream

Composition: 34%  $C_2H_4$ , 66%  $N_2$

Velocity: 35 cm/s (parabolic)

## Oxidizer stream

Composition: 21%  $O_2$ , 79%  $N_2$

Velocity: 35 cm/s (flat)

## Geometry

Fuel nozzle diameter: 4 mm

Thickness: 0.38 mm

Coflow diameter: 50 mm

R.K. Mohammed, et al., *Computational and experimental study of a forced, time-varying, axisymmetric, laminar diffusion flame*, Symposium (International) on Combustion, 27(1):693-702, 1998.

## Numerical simulation

### Axisymmetric 2D Mesh

Domain: 54 x 120 mm

Cells: ~25,000

### Kinetic mechanism

POLIMI\_C1C3\_HT\_1412

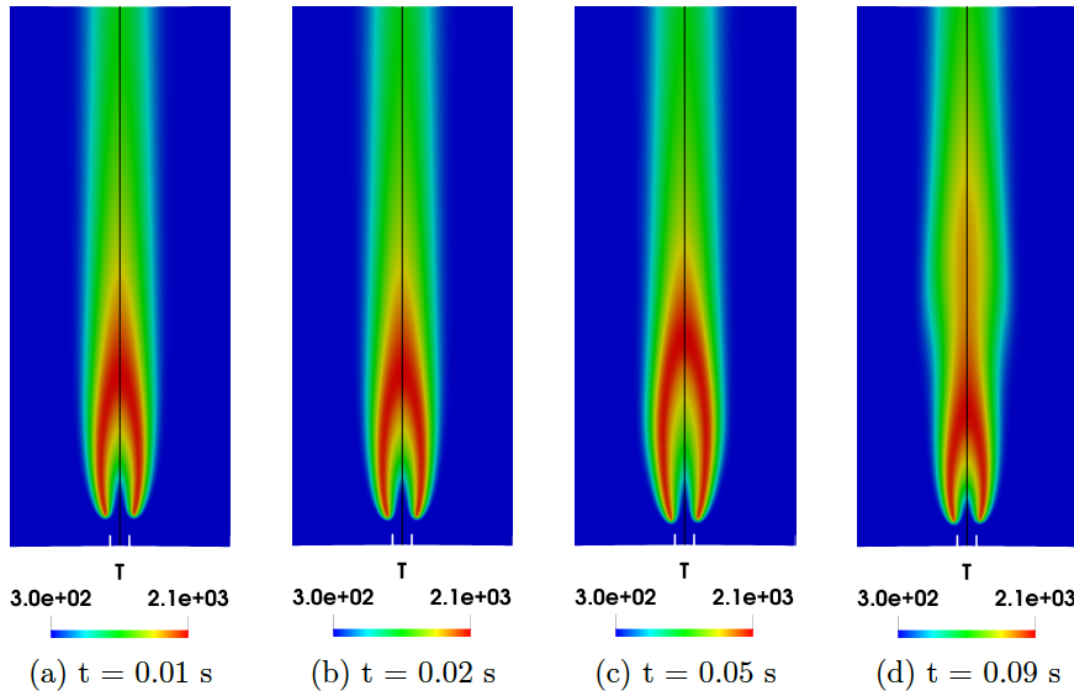
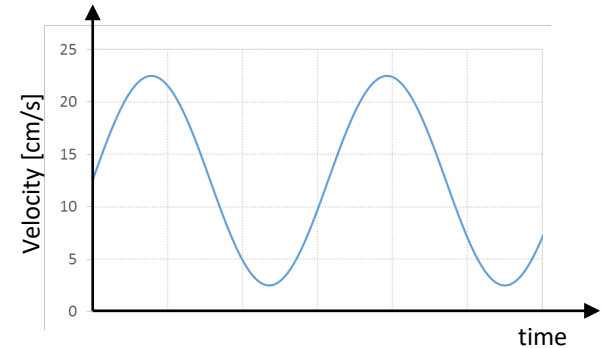
84 species and 1698 reactions

### CFD code

laminarSMOKE (based on the operator splitting approach)

The dataset was created by introducing a perturbation in the fuel inlet velocity, according to a sinusoidal function with prescribed amplitude  $A$  and frequency  $f$

$$v_{fuel}(t) = v_{fuel}^{ss} [1 + A \sin(2\pi f t)]$$



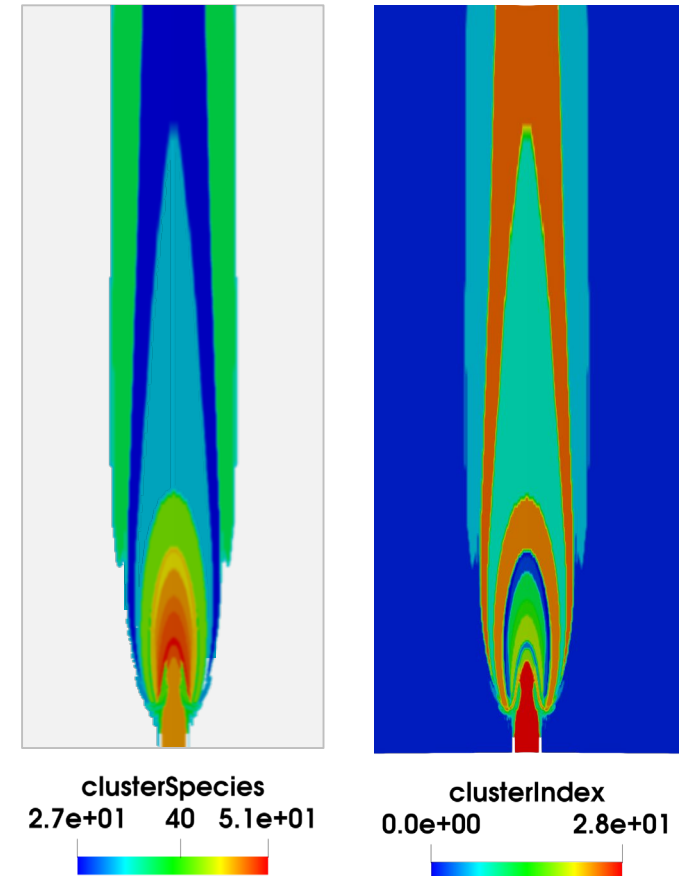
## Dataset: f10A25

A dataset with  $\sim 130,000$  observations was created by imposing a frequency of 10 Hz and an amplitude of 0.25

<https://www.kaggle.com/datasets/albertocuoci/laminar-coflow-flame-drm19-ch4n2-6535>

**DRG-EP** is applied in each cluster to generate the reduced mechanisms.

- For each sample point a reduced mechanism was generated. A single reduced mechanism for each cluster was created as the union of species and reactions corresponding to the individual reduced mechanisms of each sample point for that cluster.
- Fuel and oxidizer were assumed as target species for DRG-EP, and several **tolerance thresholds**  $\varepsilon$  were tested (0.005 to 0.1)



P. Pepiot-Desjardins, H. Pitsch, *An efficient error-propagation-based reduction method for large chemical kinetic mechanisms*, Combustion Theory and Modelling 12 (2008) 1089–1108

$\varepsilon_{DRGEP}$	$n_{sp}^{mean}$	$n_{sp}^{max}$	$\lambda_{mean}$
0.030	31	38	0.080
0.020	34	42	0.079
0.010	39	44	0.075
0.005	43	50	0.071

**Dissimilarity coefficient**  $\lambda = \frac{1}{n_{sp}} \sum_{i=1}^{n_{sp}} (1 - x_i)$       Good partitioning:  $\lambda \rightarrow 0$

$$x_i = \frac{1}{n_{obs}} \sum_{j=1}^{n_{obs}} \delta_{ij} \quad \delta_{ij} = \begin{cases} 1 & \text{If species } i \text{ is included in reaction mechanism generated by observation } j \\ 0 & \text{otherwise} \end{cases}$$

1. Steady-state flame

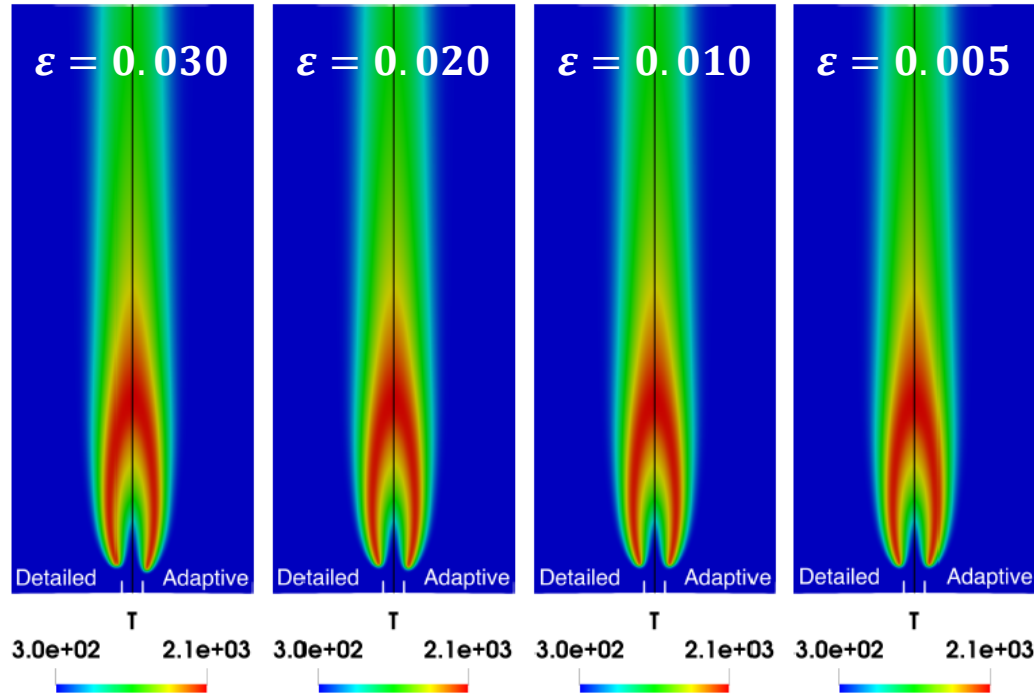
2. Unsteady flame:  $f=10\text{Hz}$ ,  $A=0.25$

Same data used for training  
(Testing purposes only)

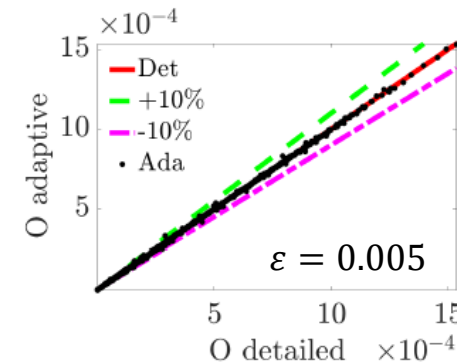
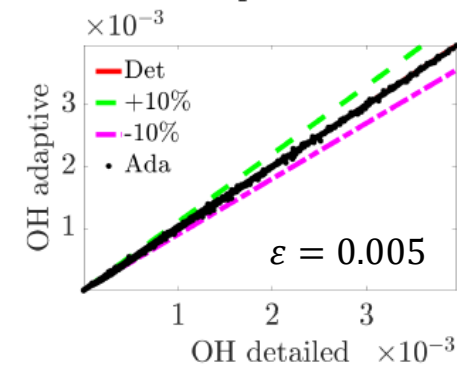
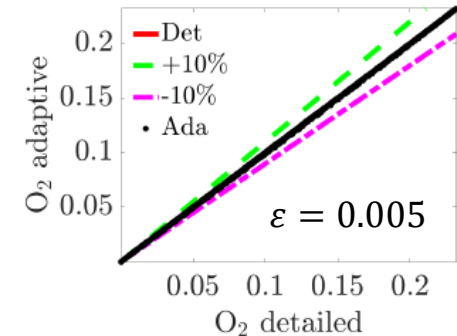
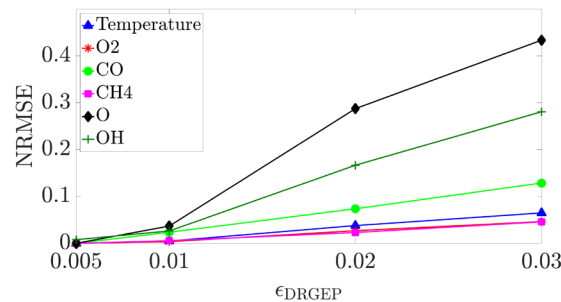
3. Unsteady flames:  $f=10, 40, 80\text{ Hz}$ ,  $A = 0.50, 0.75, 0.90$

**! Exploration of new conditions not included in the training dataset**

# Results: steady-state flame

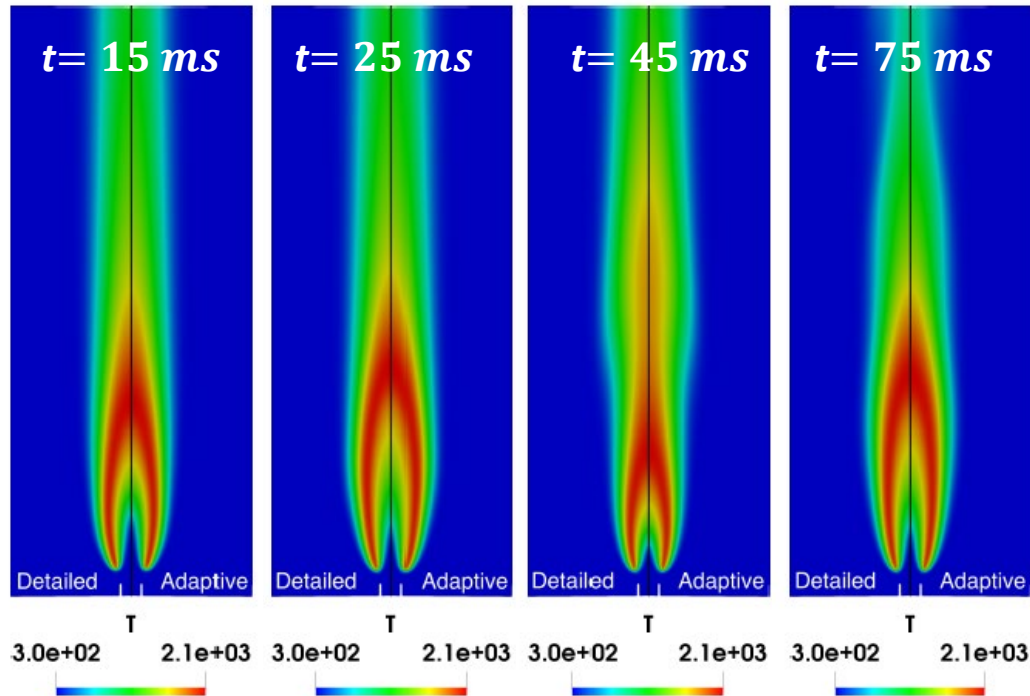


$\epsilon_{DRGEP}$	Speed-up
0.030	5.4
0.020	4.9
0.010	4.6
0.005	4.0



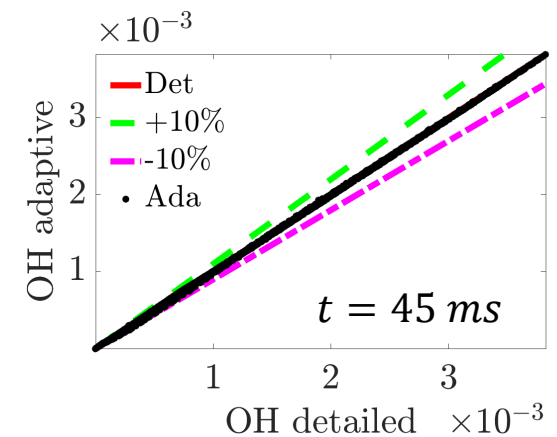
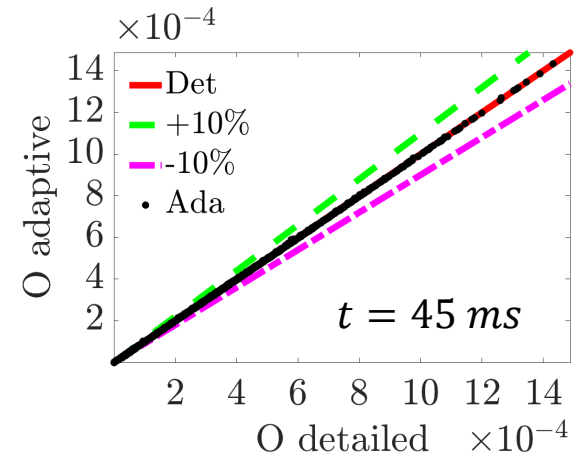


# Results: unsteady flames



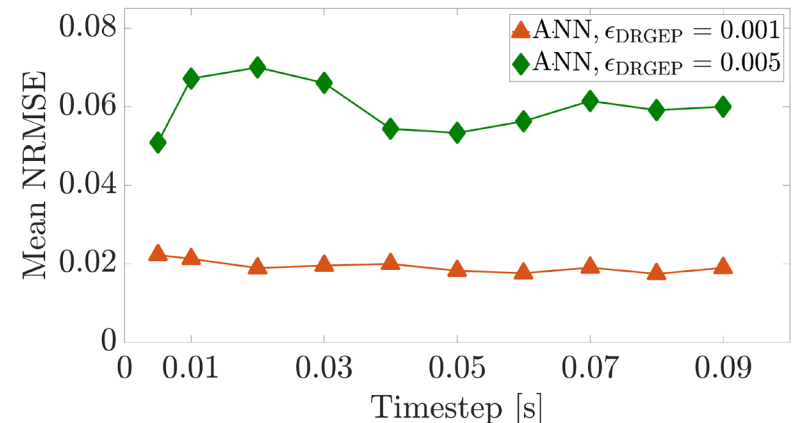
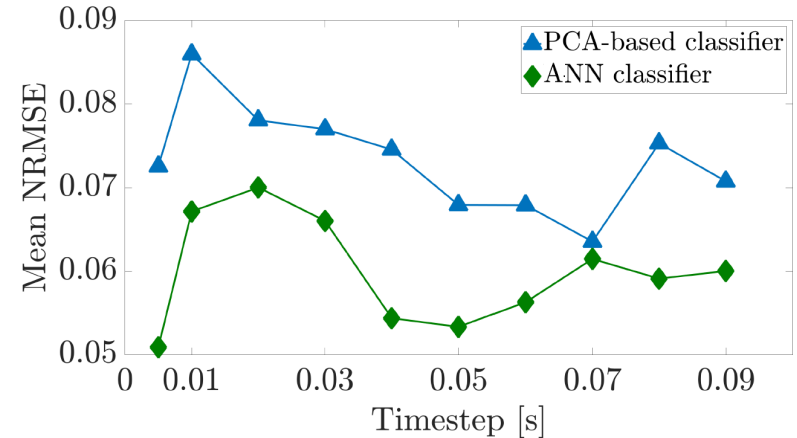
Same training dataset  
f10A25  
 $\varepsilon = 0.005$

New conditions  
 $f = 20 \text{ Hz}$   
 $A = 0.25$



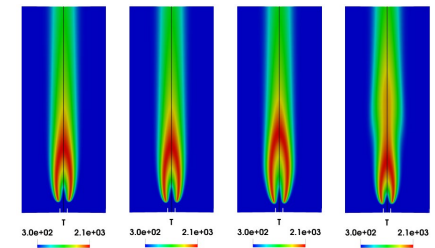
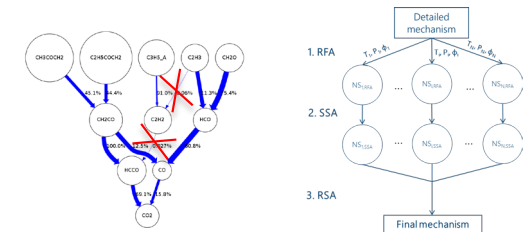
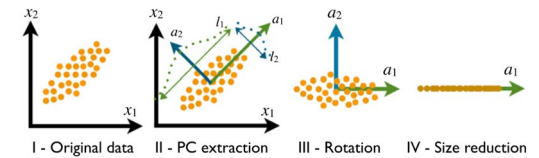
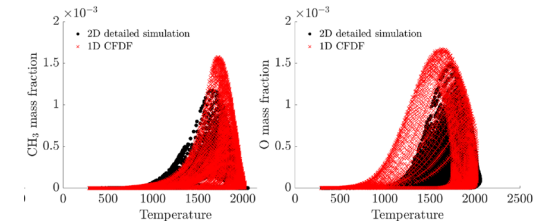
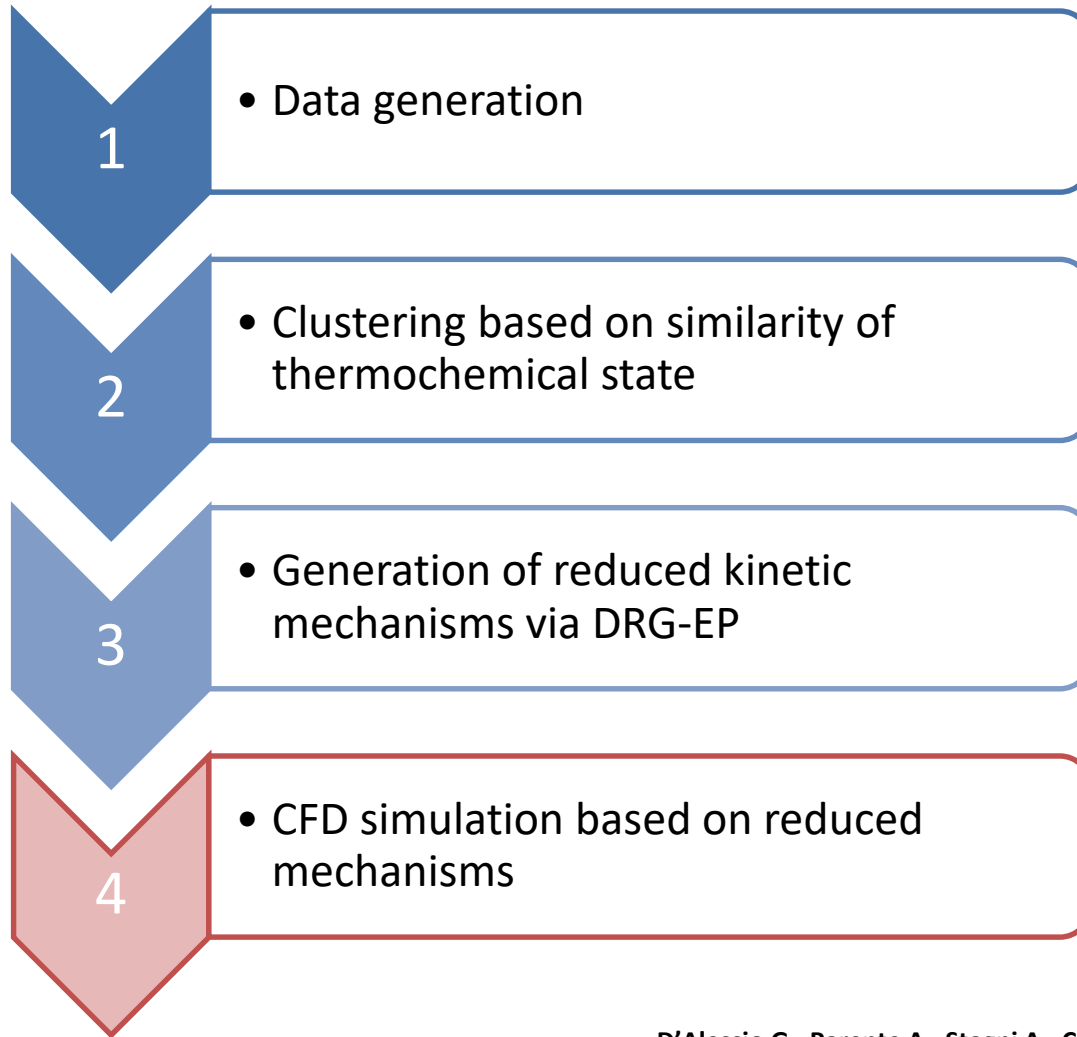
- The ANN used for the classification consisted of **2 hidden layers with 200 and 400 neurons**, respectively, chosen after an optimization of the hyper-parameters to achieve a satisfactory accuracy in the class prediction.
- The activation functions chosen for the hidden layers were both **ReLU (Rectified Linear Unit)**, with a **softmax activation** for the output layer as required in case of multi-class classification tasks.

Averaged normalized root mean square error over time

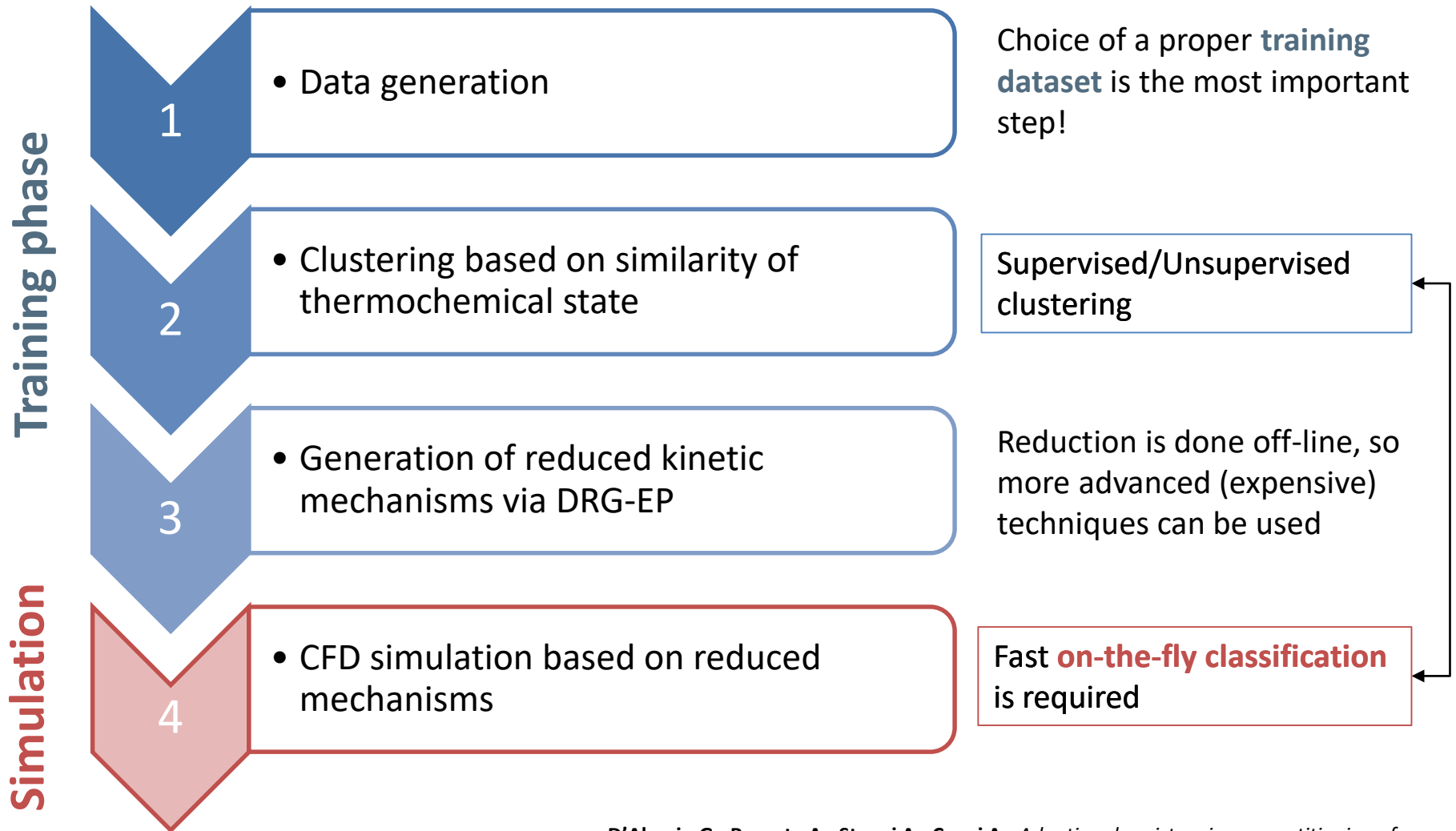


Training phase

Simulation

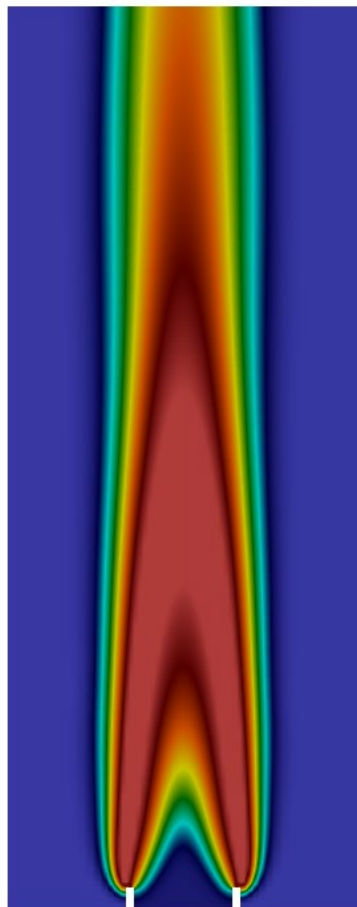


D'Alessio G., Parente A., Stagni A., Cuoci A., *Adaptive chemistry via pre-partitioning of composition space and mechanism reduction*, Combustion and Flame, 211, p. 68-82 (2020)



D'Alessio G., Parente A., Stagni A., Cuoci A., *Adaptive chemistry via pre-partitioning of composition space and mechanism reduction*, Combustion and Flame, 211, p. 68-82 (2020)

# A test case: $nC_7H_{16}/CH_4/N_2$ laminar flame



## Fuel stream

Composition: 2.47%  $nC_7H_{16}$ ,  
48.7%  $CH_4$ , 48.7%  $N_2$   
Velocity: 10.12 cm/s (parabolic)

## Oxidizer stream

Composition: 21%  $O_2$ , 79%  $N_2$   
Velocity: 12.32 cm/s (flat)

## Geometry

Fuel nozzle diameter: 11 mm  
Thickness: 0.90 mm  
Coflow diameter: 50 mm

## Axisymmetric 2D Mesh

Domain: 40 x 100 mm  
Cells: ~10,000

## Kinetic mechanism

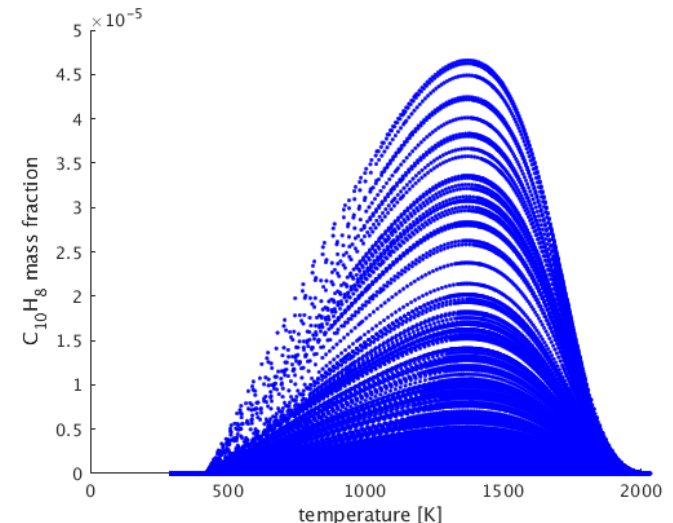
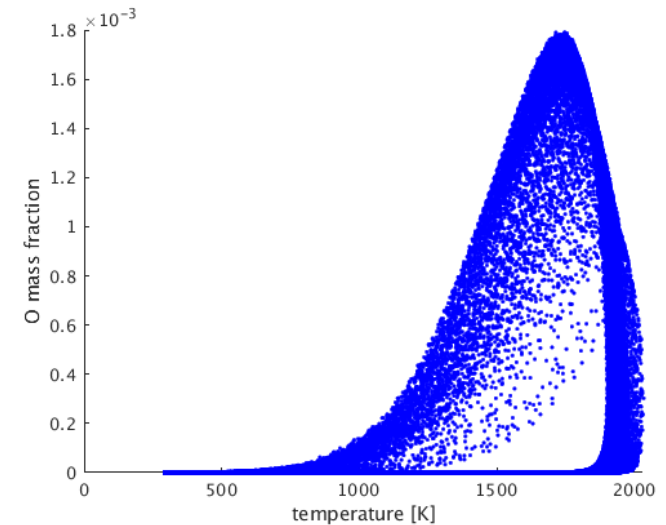
POLIMI\_PRF\_PAH\_HT\_1412  
176 species and 6067 reactions

## CFD code

laminarSMOKE (based on the  
operator splitting approach)

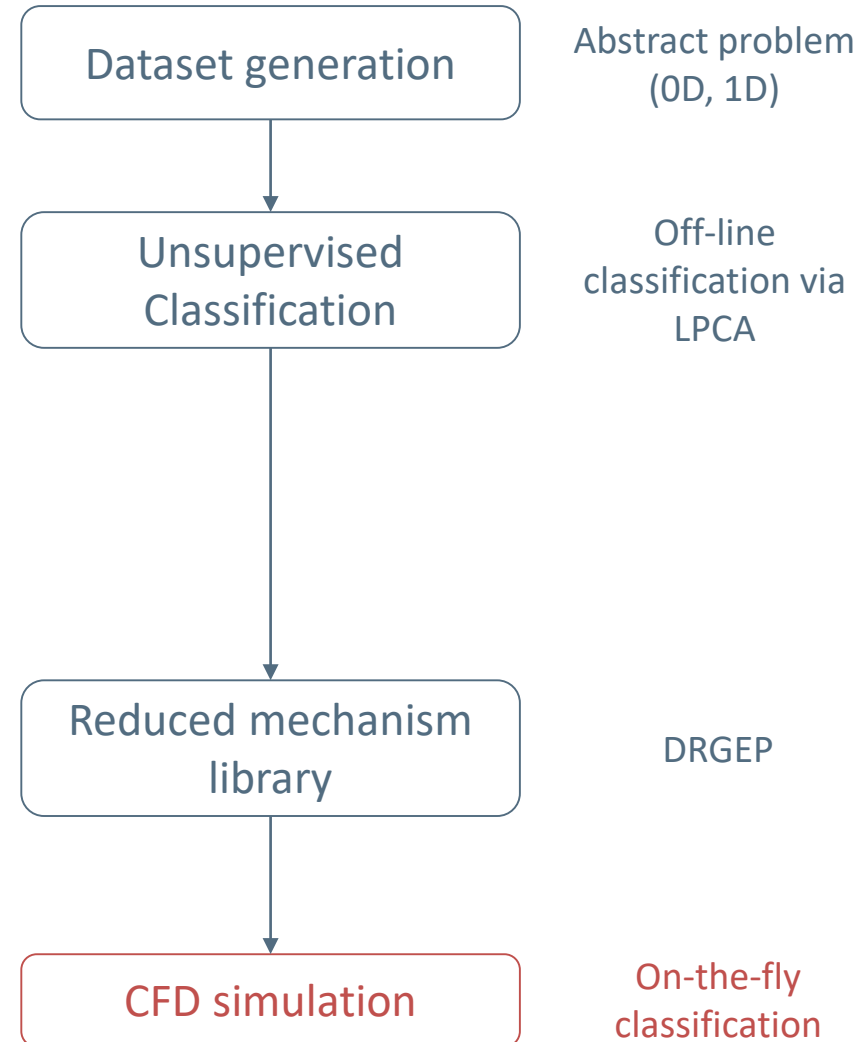
M. Kashif et al., *Sooting propensities of some gasoline surrogate fuels: Combined effects of fuel blending and air vitiation*, Combustion and Flame, 162(5):1840–1847, 2015

- The generated data set must cover adequately the composition space that is expected to be visited during the simulation of the system under investigation
- The samples were generated by means of **1D counterflow diffusion flames (CFDF)**, adopting a wide range of strain rates randomly chosen from 15 to 1000 1/s (i.e., from **thermodynamic equilibrium to extinction**)
- The resulting data set consists of about 220,000 observations, corresponding to ~100 different CFDF flames.



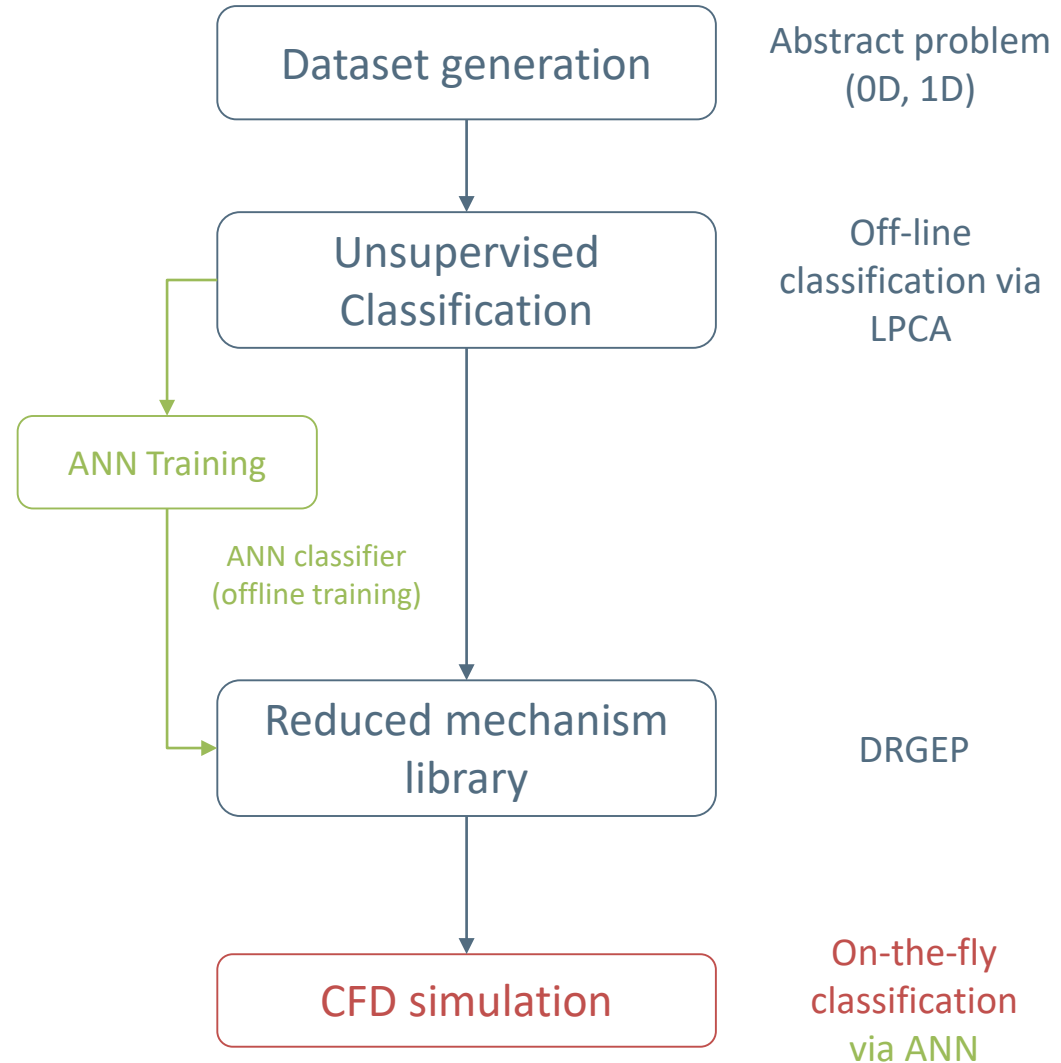
- If the chemical mechanism consists of a large number of species, the classification can be a difficult task to accomplish since the **use of distances in high-dimensional spaces can sometimes lead to poor results** (Aggarwal, 2001)
- **ANN** represent a valid alternative to improve the classification efficiency, as they do not rely on the use of the metrics in high-dimensional spaces

D'Alessio G., Cuoci A., Parente A., *Feature extraction and artificial neural networks for the on-the-fly classification of high-dimensional thermochemical spaces in adaptive-chemistry simulations*, Data-Centric Engineering (2020)



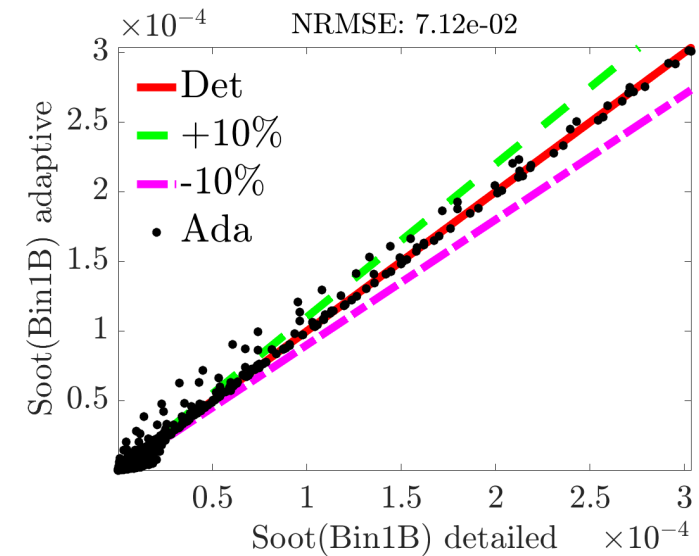
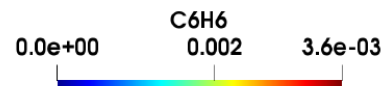
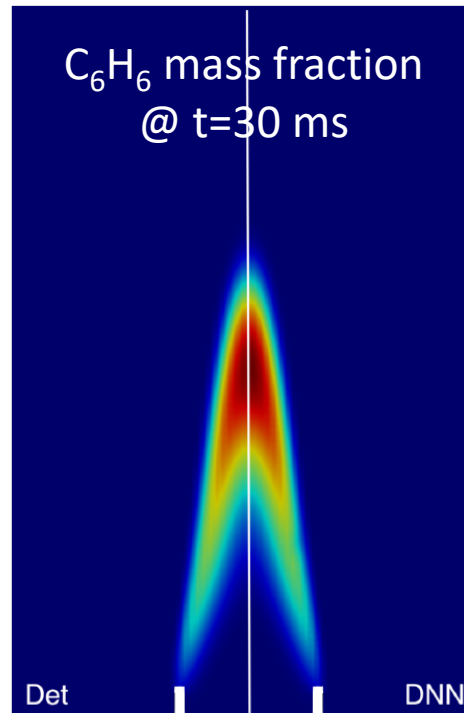
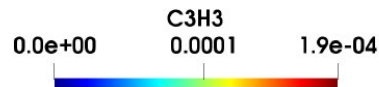
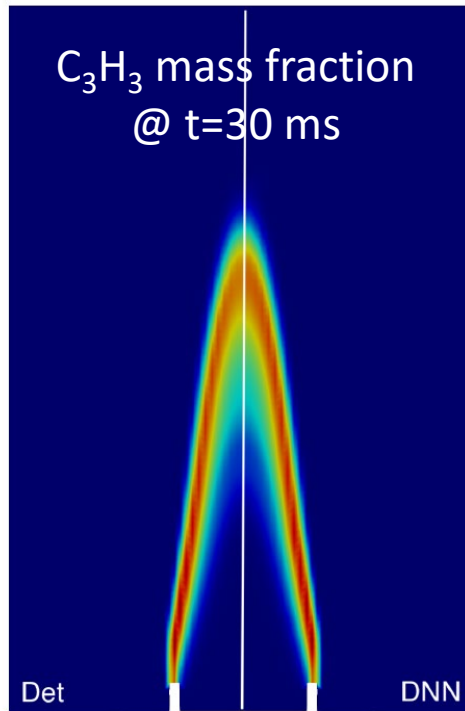
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D'Alessio G., Cuoci A., Parente A., *Feature extraction and artificial neural networks for the on-the-fly classification of high-dimensional thermochemical spaces in adaptive-chemistry simulations*, Data-Centric Engineering (2020)





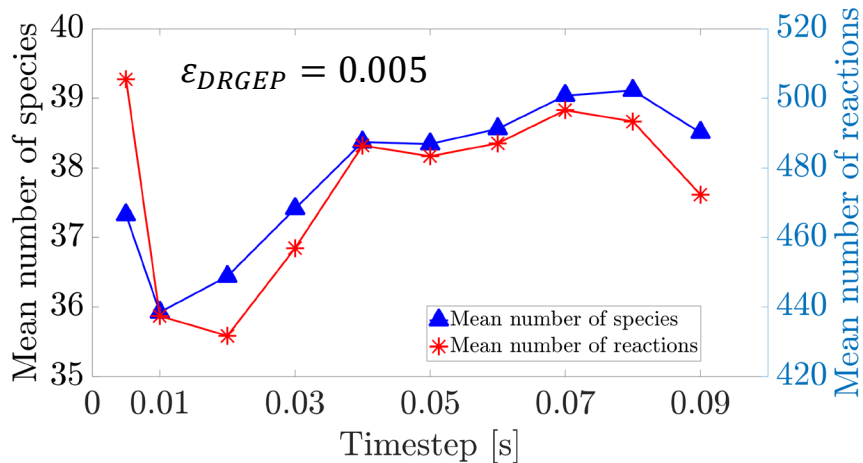
# Results: comparison with full-chemistry



BIN1B ( $C_{20}$ ) is the heaviest species in the mechanism, and it is a soot precursor

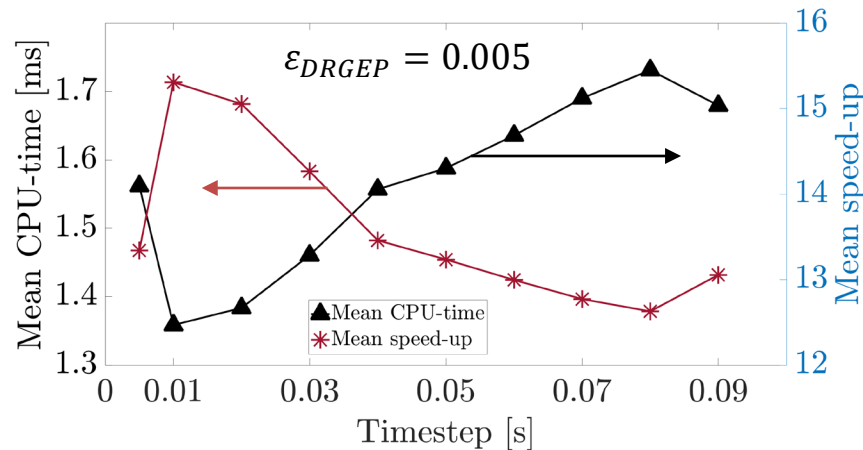
A satisfactory level of agreement is observed not only for main species, but also for radicals (such as propargyl) and heavy species (such as benzene and soot precursors).

# Results: speed-up



The reduction in terms of number of species is remarkable (about 50%).

A stronger reduction in the number of active reactions is evident: less than 10% of the original reactions are retained.



The **speedup factor** changes in time because the number of species and reactions can also change in time depending on the local flame chemistry

